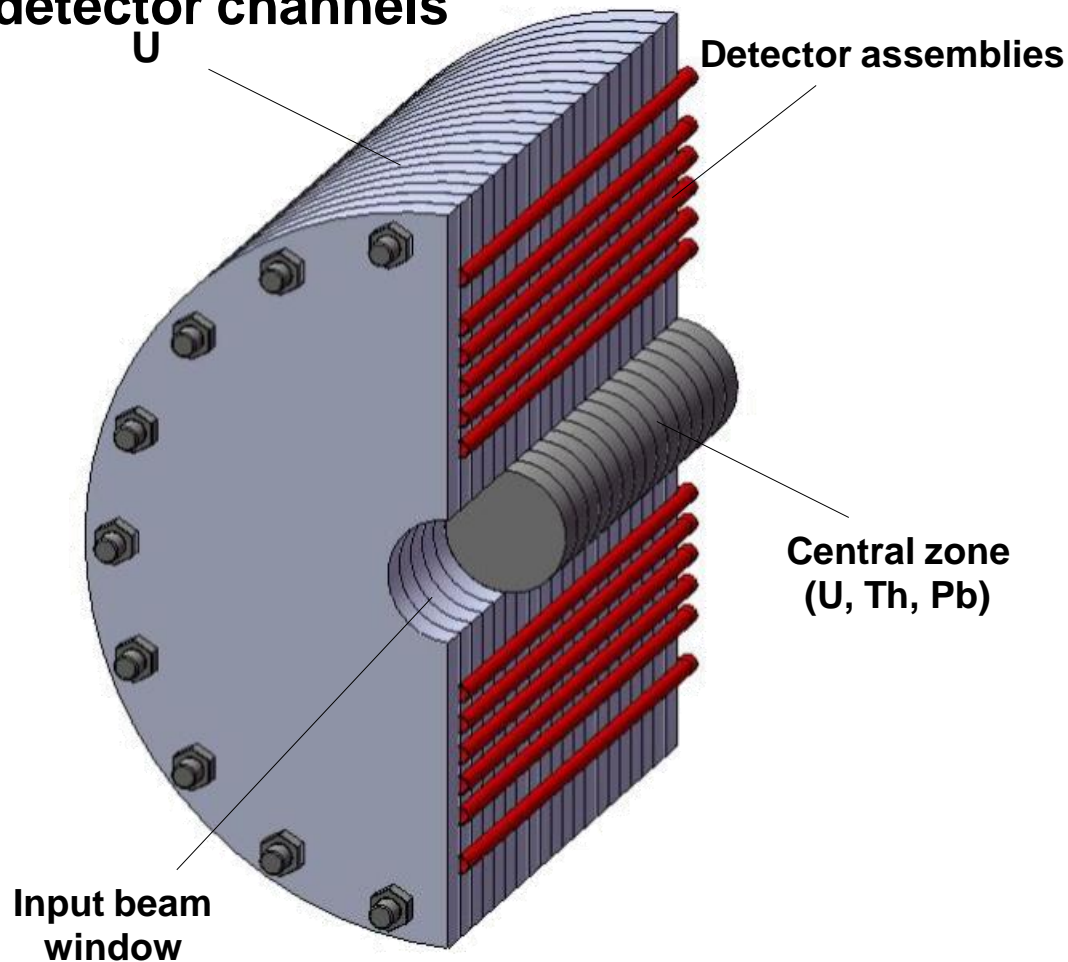


Comparison of the spallation neutron field on the surface of Carbon and Lead Target under 660 MeV protons irradiation

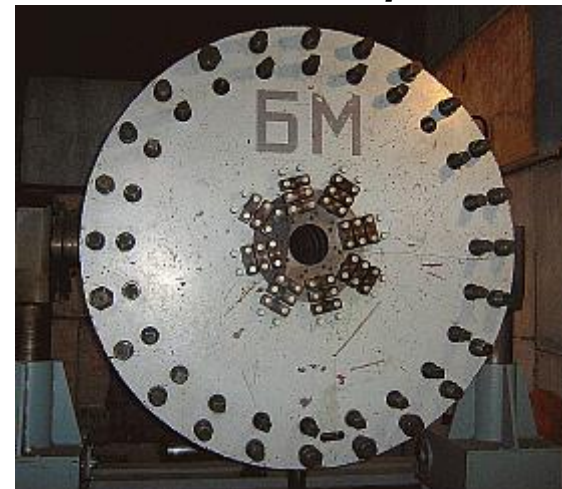
J.Adam, L. Zavorka, A.A.Baldin, W.Furman, S.Gustov, K.Katovsky,
J.Khushvaktov, D.Kral, A.Solnyshkin, J.Svoboda, P.Tichy,
S.Tyutyunnikov, J.Vrzalova, V.Wagner, M. Zeman

Quasi-infinite depleted uranium target (BURAN) with replacement central zone

Longitudinal section of TA BURAN together with central zone and detector channels



Front view photo



Rear view photo





CARBON TARGET

10 discs with diameter 190 mm and thickness 100 mm

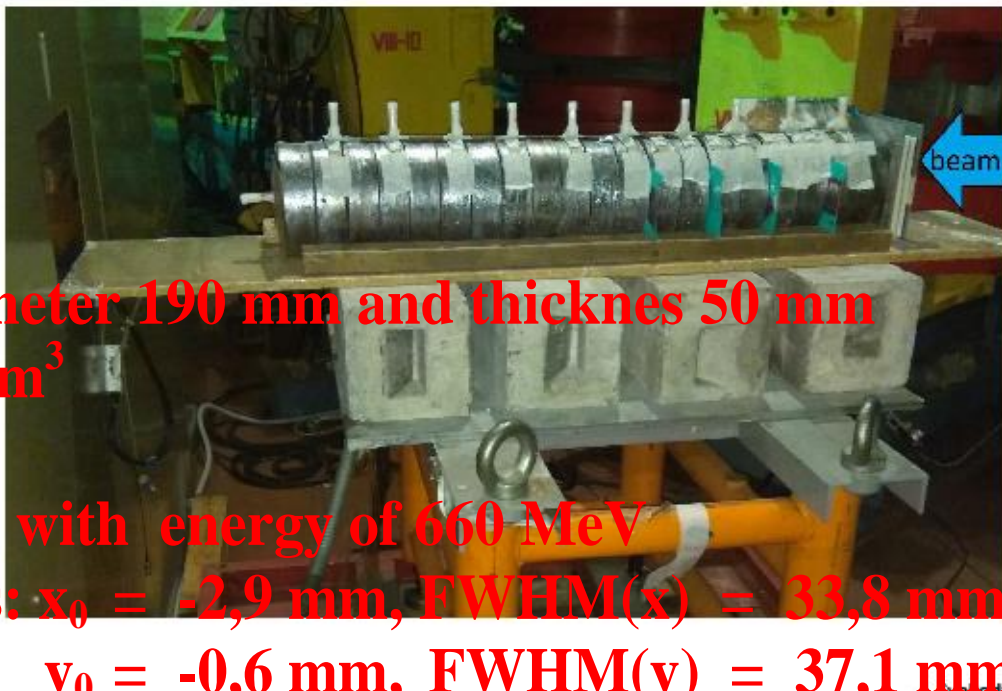
Density $1,8 \text{ g/cm}^3$, admixtures $< 0,02\%$

PROTON BEAM with energy of 660 MeV

Beam parameters: $x_0 = -5,1 \text{ mm}$, $\text{FWHM}(x) = 35,1 \text{ mm}$

$y_0 = -0,1 \text{ mm}$, $\text{FWHM}(y) = 34,6 \text{ mm}$

LEAD target setup



LEAD TARGET

20 discs with diameter 190 mm and thicknes 50 mm

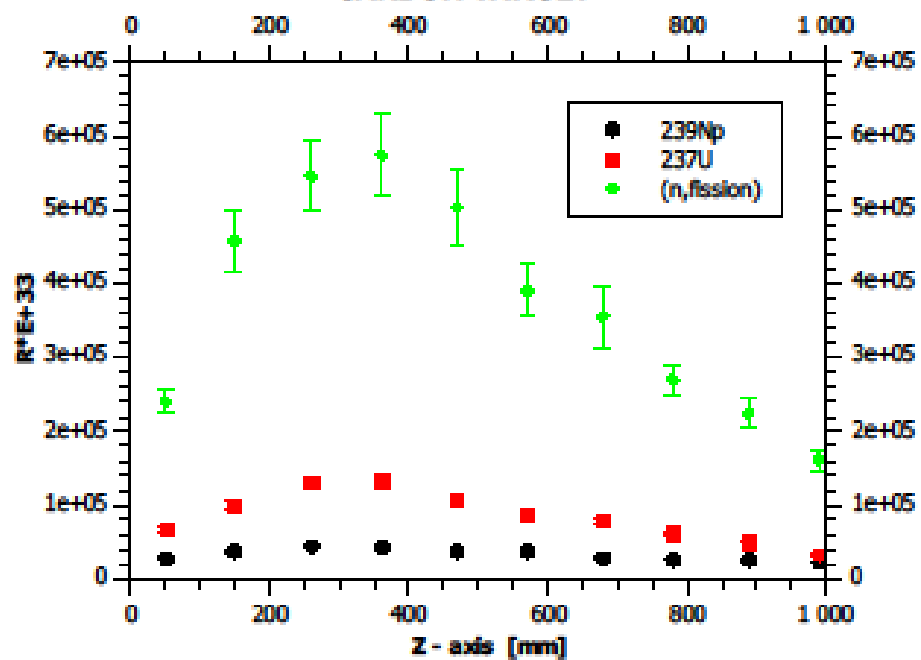
Density 11,35 g/cm³

PROTON BEAM with energy of 660 MeV

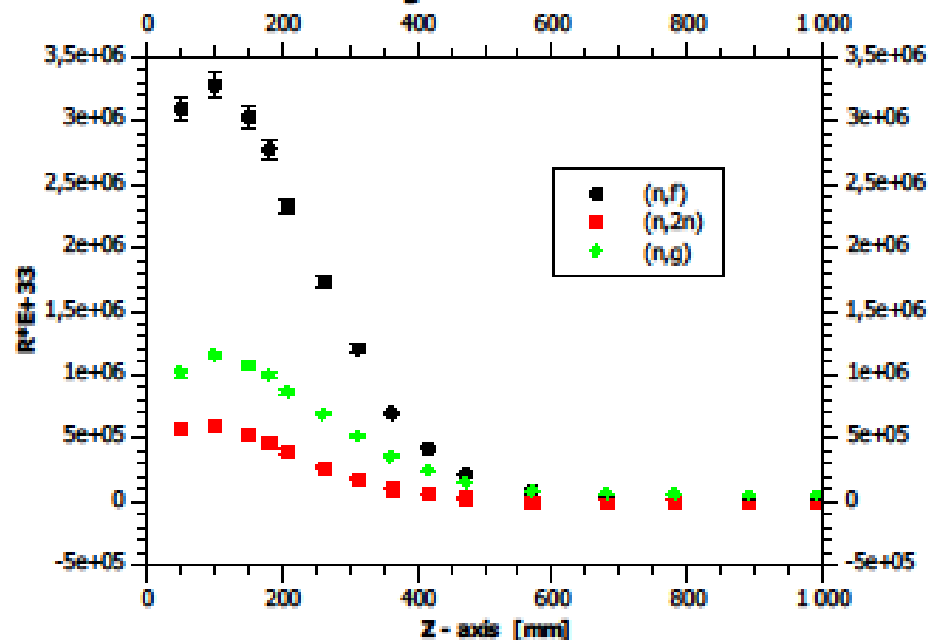
Beam parameters: $x_0 = -2,9$ mm, FWHM(x) = 33,8 mm

$y_0 = -0,6$ mm, FWHM(y) = 37,1 mm

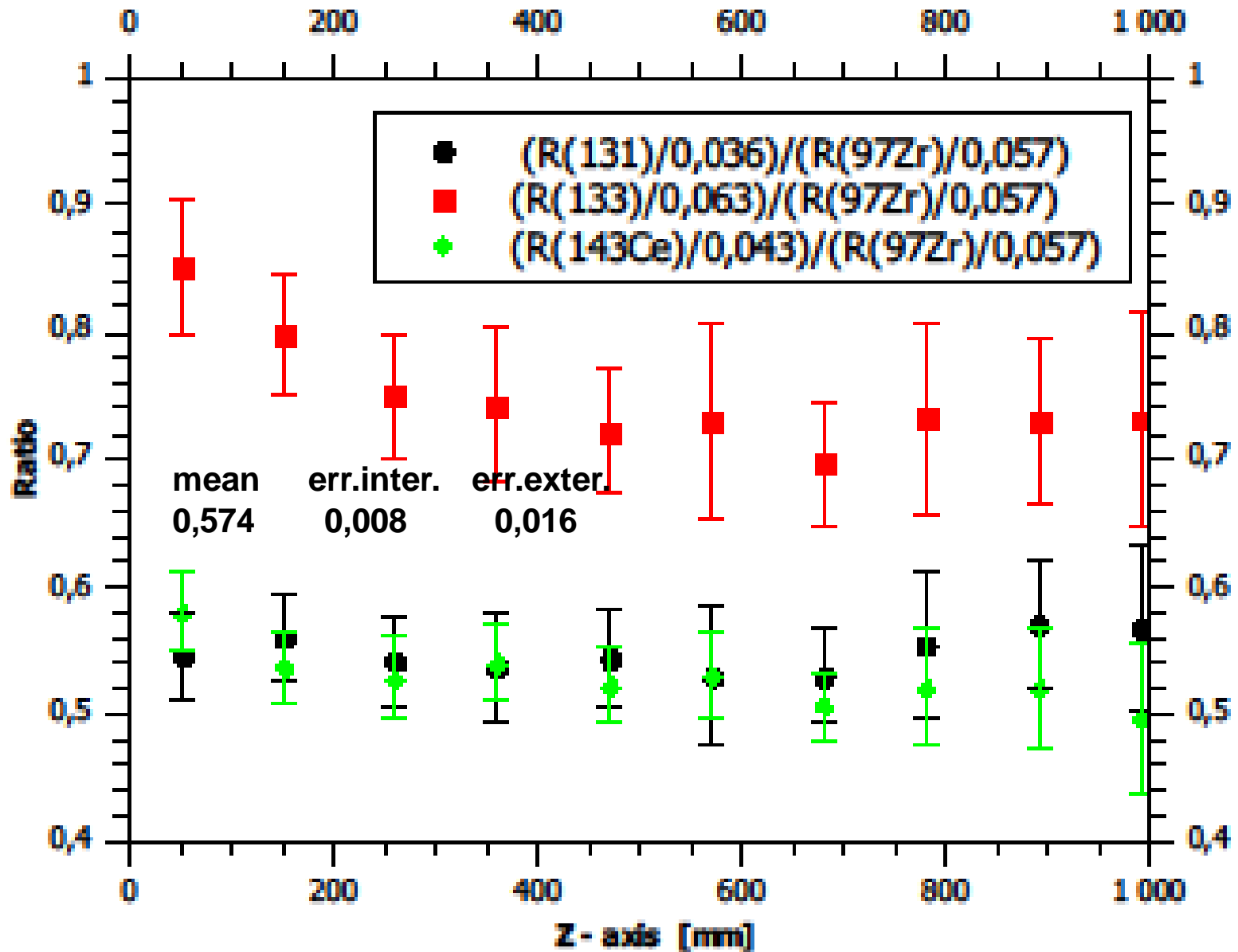
CARBON TARGET



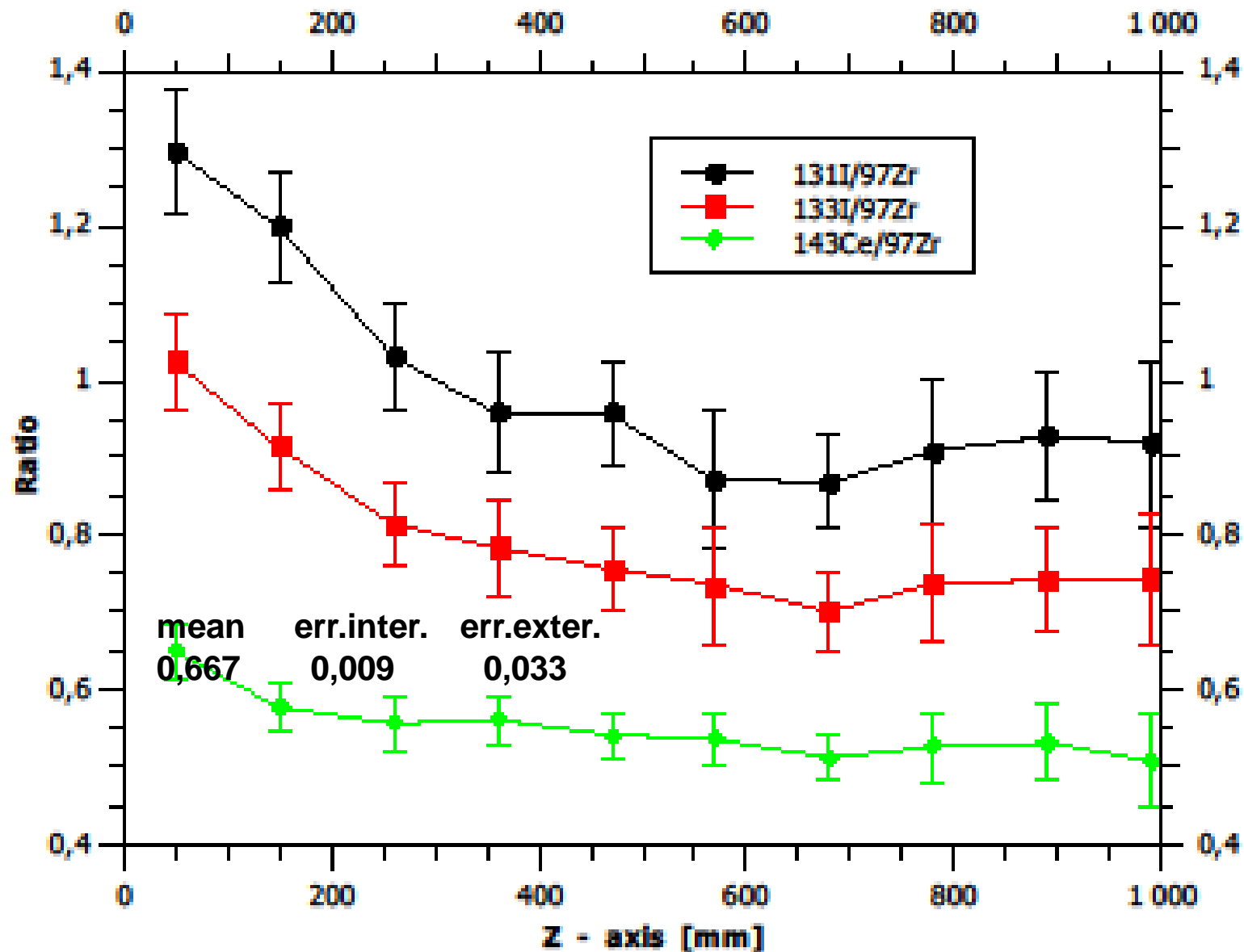
Lead Target Ud on surface



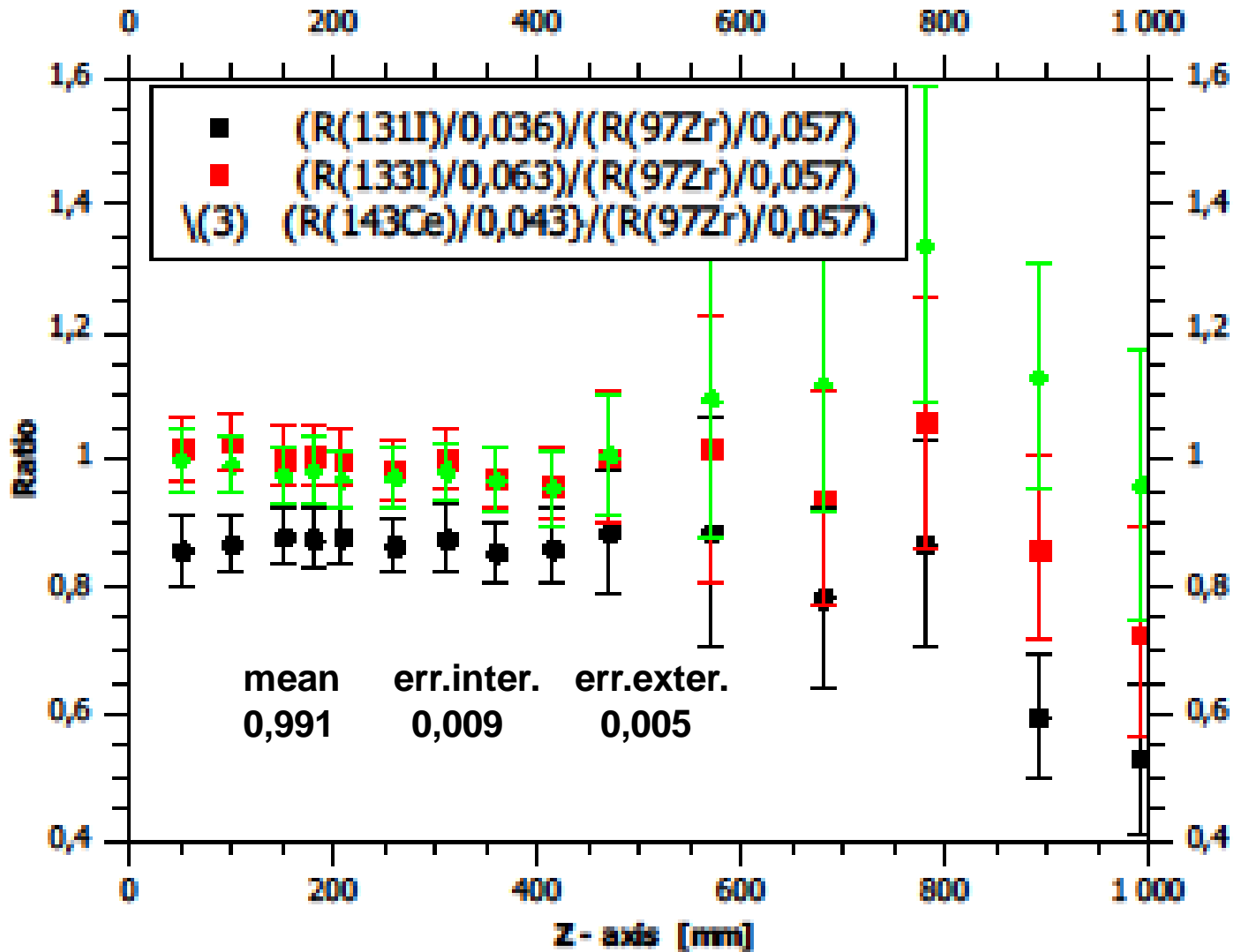
Ratio $(R(I)/Y(I))/(R(97Zr)/0,057)$ Carbon Target



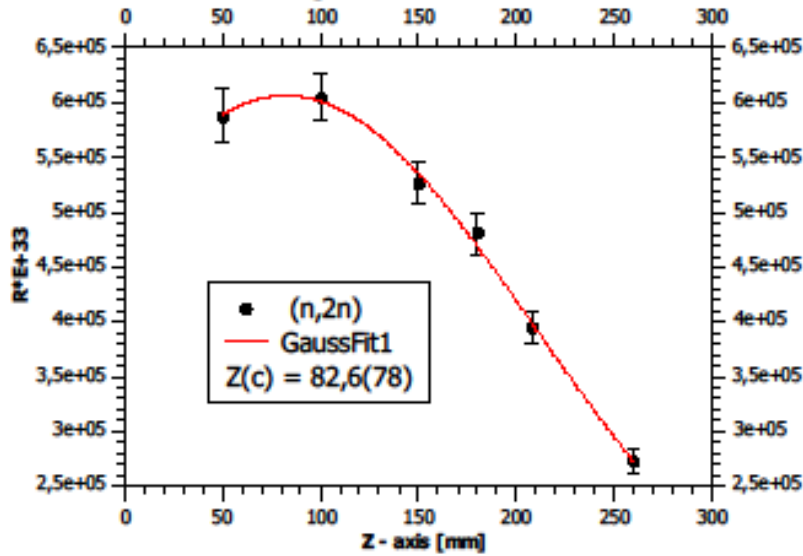
Ratio (R(x)/yield(x)/(R(Zr)/yield(Zr))) Carbon yield calcul



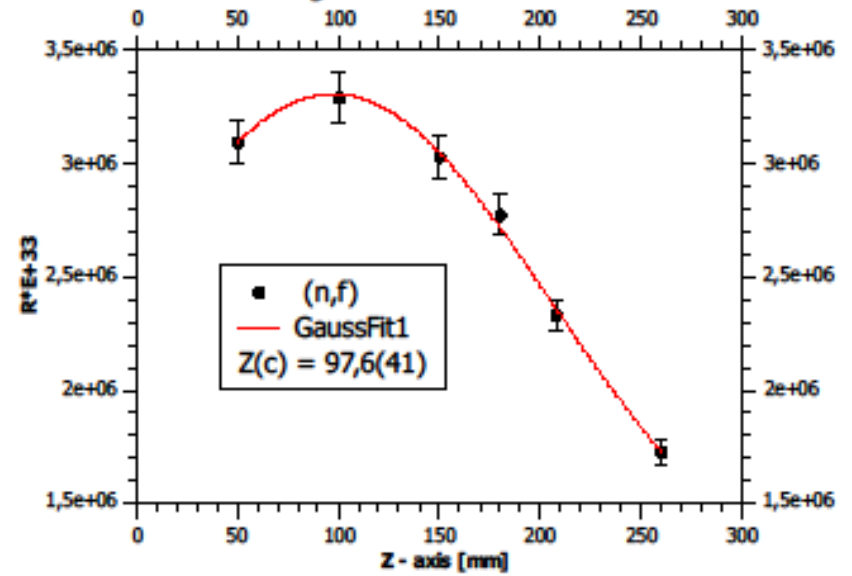
Ratio (R(I)/Y(I))/(R(97Zr)/0,057) Lead Target



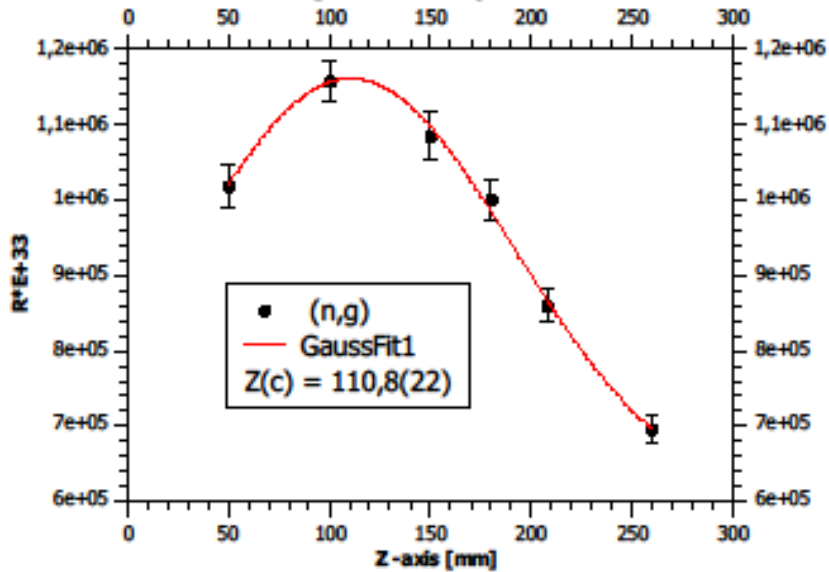
Lead Target Ud 237U 08062018



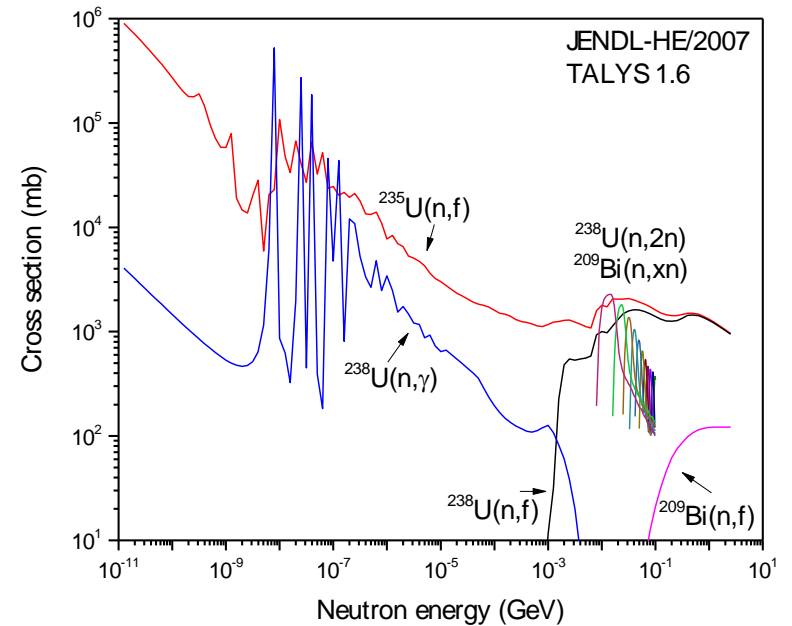
Lead Target Ud fission 6 08062018



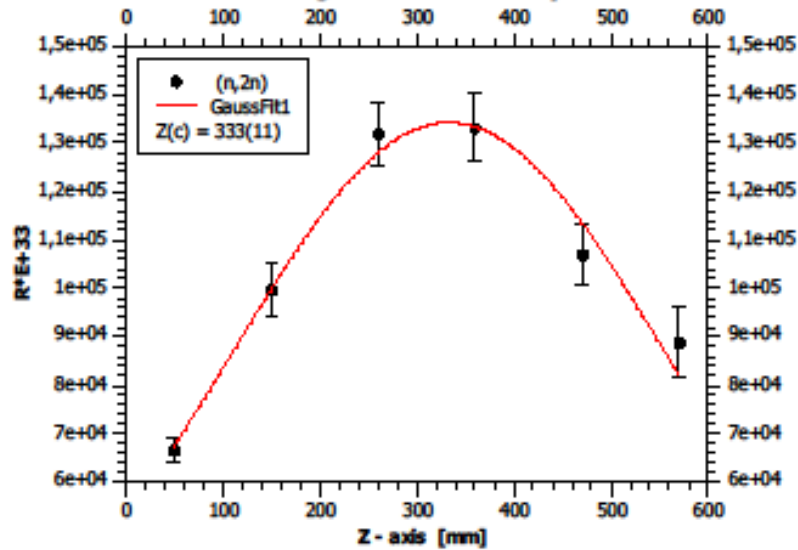
Lead Target Ud 239Np 08062018



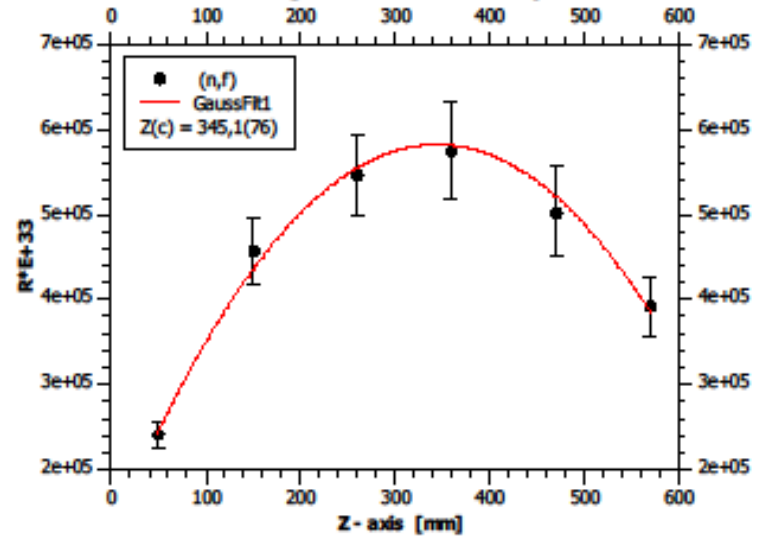
Fundamental cross sections



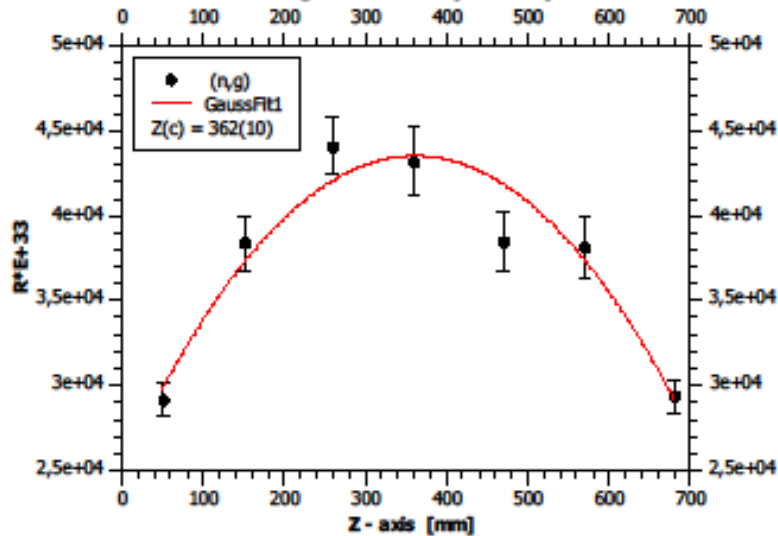
Carbon Target Ud 237U 25May2018

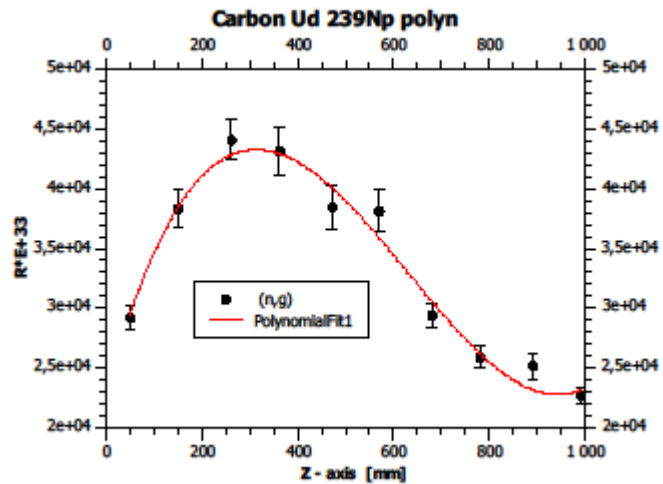
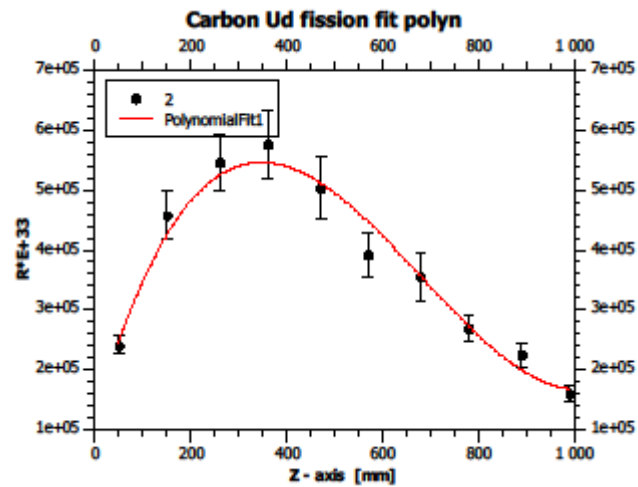
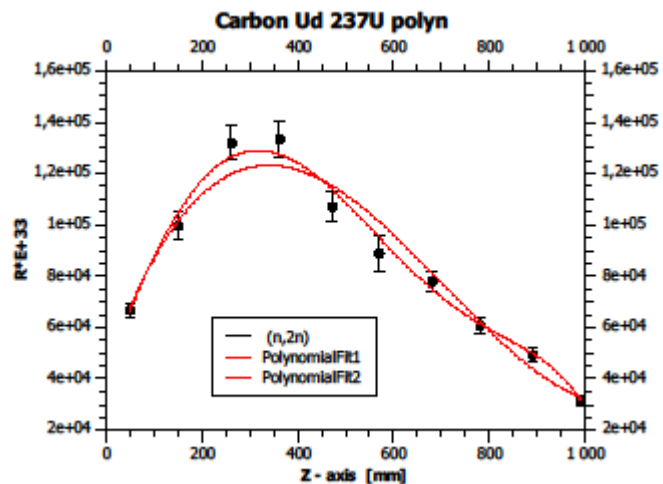


Carbon Target Ud fission 25May2018

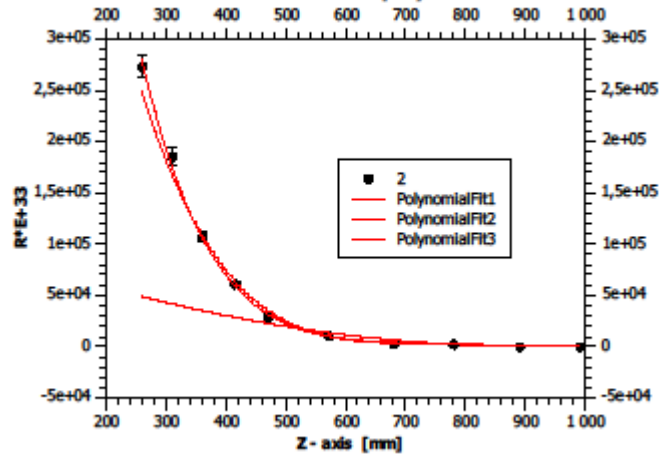


Carbon Target Ud 239Np 25May2018

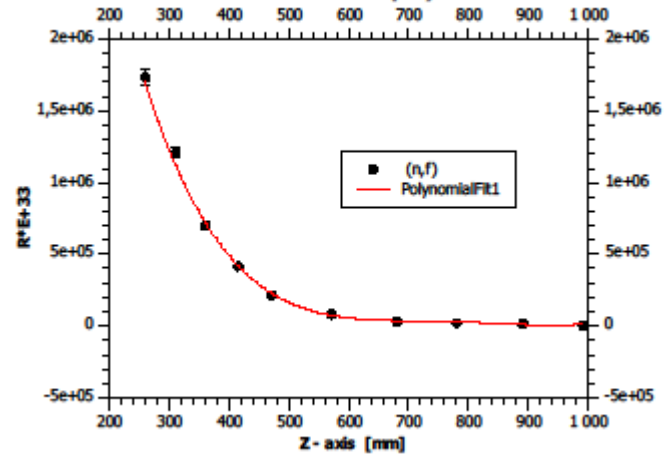




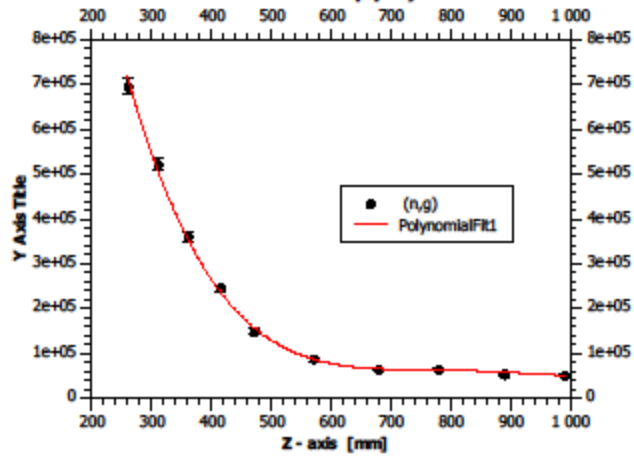
Lead Ud 237U polyn



Lead Ud fission polyn



Lead Ud 239Np polyn



CARBON TARGET

Gauss Fit: $y_0 + A * \text{sqrt}(2/\pi) / w * \exp(-2 * ((x-x_c) / w)^2)$

From x = 50 mm to x = 990 mm

Reaction	A(area)	z _c (center)	w (width)
U _d (n,2n)	9,3(38)E7	403(23)	692(160)
U _d (n,f)	2,24(44)E8	406(22)	452(71)
U _d (n,f)new	2,73(66)E8	417(27)	427(82)
U _d (n,γ)	1,14(13)E7	355(14)	426(38)

Polynomial Fit : $a_0 + a_1 * x + a_2 * x^2 + a_3 * x^3$

From x = 50 mm to x = 990 mm

	a ₀	a ₁	a ₂	a ₃
U _d (n,2n)	4,37(40)E4	5,23(45)E2	-1,02(10)	4,80(58)E-4
U _d (n,f)	1,21(25)E5	2,76(32)E3	-5,33(73)	2,62(44)E-3
U _d (n,f)new	1,14(63)E5	3,93(74)E3	-7,4 (17)	3,6(10)E-3
U _d (n,γ)	2,28(14)E4	1,46(14)E2	-0,31(3)	1,65(18)E-4

Integral = $\{ a_0 * x + a_1 * x^2 / 2 + a_2 * x^3 / 3 + a_3 * x^4 / 4 \}_0^{1000}$

Integral	Fission old	Fission new	(n,2n)	(n,γ)
Gauss	3,696E-25	4,971E-25	8,669E-26	3,374E-26
Polynom	3,827E-25	5,093E-25	8,693E-26	3,364E-26
Average	3,762E-25	5,032E-25	8,681E-26	3,369E-26

LEAD TARGET

Gauss Fit: $y_0 + A * \text{sqrt}(2/\pi) / w * \exp(-2 * ((x-x_c) / w)^2)$

From x = 50 mm to x = 260 mm

Reaction	A(area)	z _c (center)	w (width)
U _d (n,2n)	1,65(59)E8	82,6(78)	251(46)
U _d (n,f)	6,3(16)E8	97,6(41)	216(30)
U _d (n,γ)	1,13(13)E8	110,8(22)	160(12)

Polynomial Fit : $a_0 + a_1 * x + a_2 * x^2 + a_3 * x^3 + a_4 * x^4$

From x = 260 mm to x = 990 mm

	a ₀	a ₁	a ₂	a ₃	a ₄
U _d (n,2n)	1,20(4)E6	-6,03(21)E3	11,3(4)	-9,40(40)E-3	2,91(13)E-6
U _d (n,f)	8,63(26)E6	-4,45(16)E4	85,9(37)	-7,33(36)E-2	2,33(13)E-5
U _d (n,γ)	3,09(15)E6	-1,48(10)E4	26,8(25)	-2,15(26)E-2	6,42(98)E-6

Integral = $\{ a_0 * x + a_1 * x^2 / 2 + a_2 * x^3 / 3 + a_3 * x^4 / 4 + a_4 * x^5 / 5 \}_{260}^{1000}$

Integral	Fission	(n,2n)	(n,γ)
Gauss	7,275E-25	1,103E-25	2,555E-25
Polynom	1,911E-25	2,794E-26	2,836E-26
Sum	9,187E-25	1,383E-25	3,713E-25

The experimental rates of reactions

	$U_d(n, \text{fission})$	$U_d(n, 2n)$	$U_d(n, \gamma)$
CARBON TARGET	5,093E-25	8,693E-26	3,364E-26
LEAD TARGET	9,187E-25	1,383E-25	3,713E-25
Ratio C/L	0,554	0,629	0,091

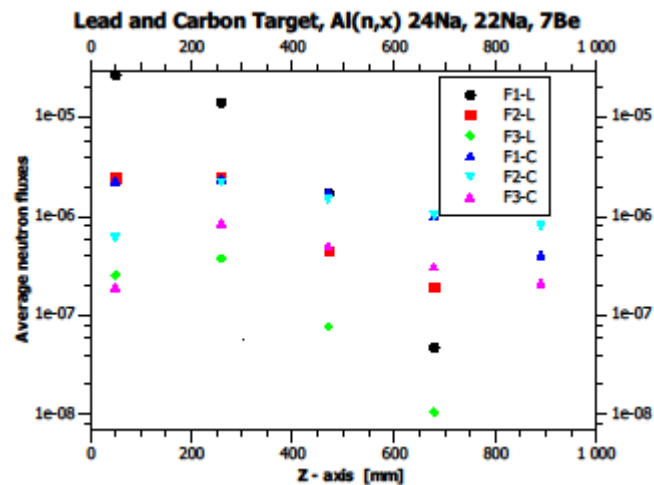
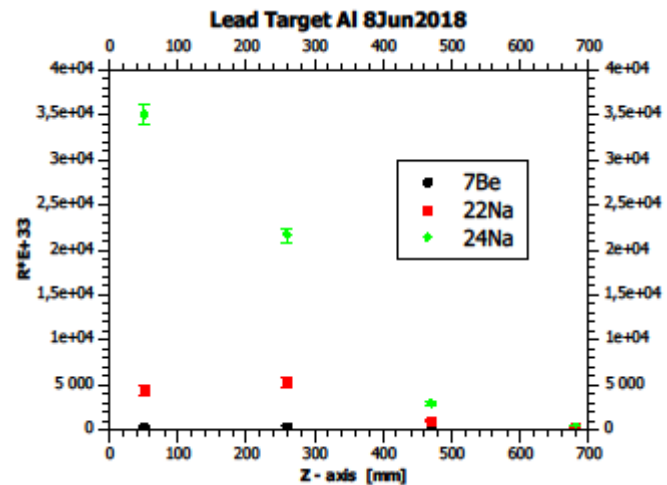
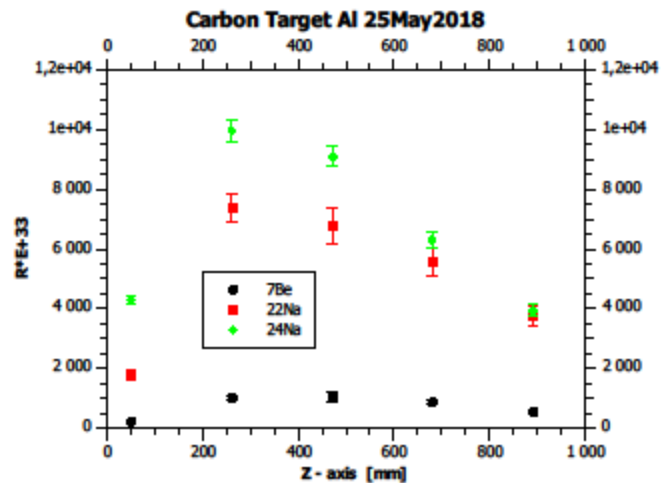
CALCULATION

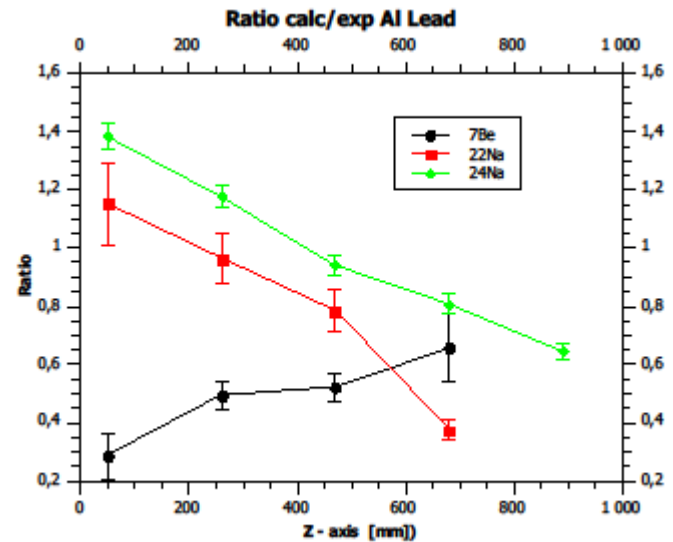
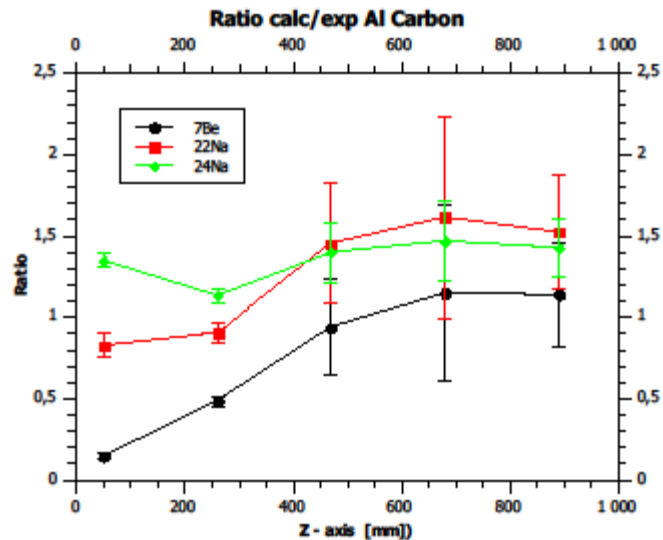
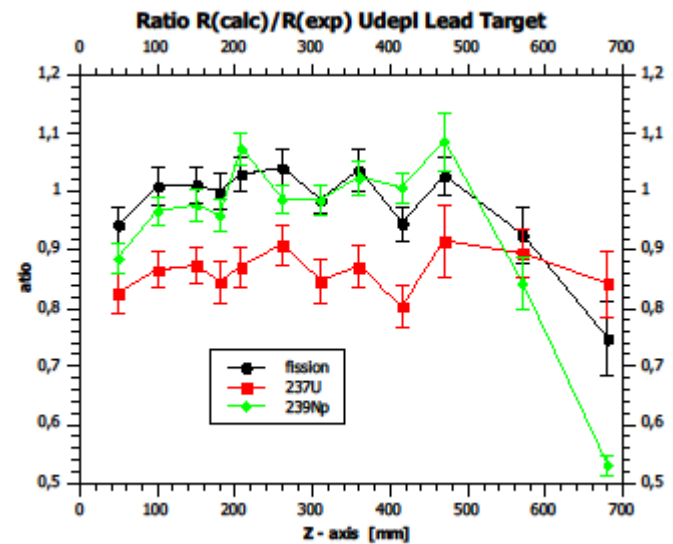
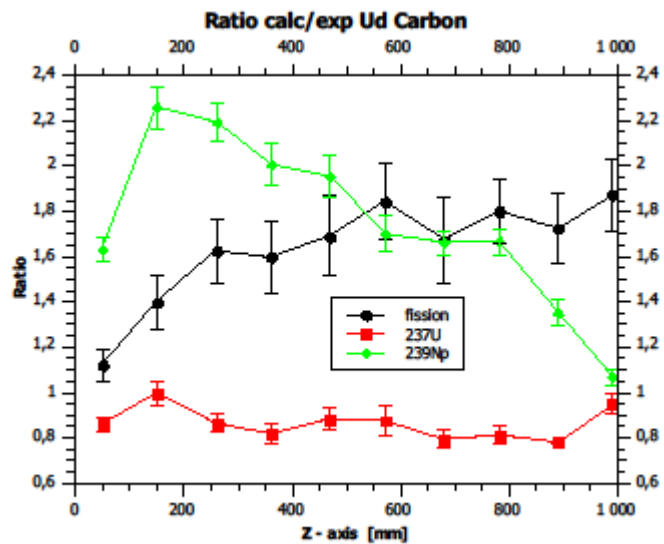
The reaction rates and the neutron fluxes were calculated with the radiation transport code **MCNPX2.7.0**
The cross sections were extracted from the intranuclear cascade model **INCL4.2**, from **TALYS-1.8** code, and the evaluated nuclear data file **TENDL-2015s**.

CARBON TARGET

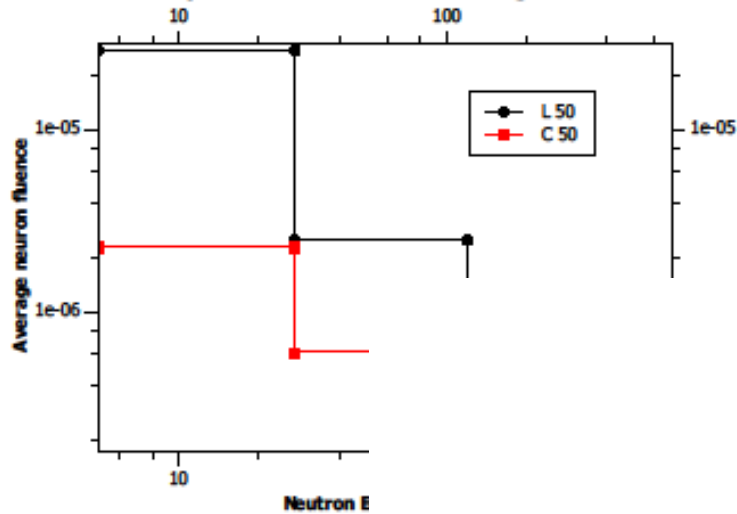
Dist. [mm]	Fis. – n [%]	Fis. – p [%]	<En> [MeV]	<Ep> [MeV]	N yield [%]	P yield [%]	YIELD* [%]
50	91	9	19,5	86,8	5,15	2,86	4,95
150	78	22	27,7	135,4	4,83	2,74	4,37
260	70	30	34,5	184,4	4,66	2,82	4,10
360	67	33	38,6	201,0	4,49	2,77	3,93
470	65	35	41,4	206,8	4,49	2,77	3,89
570	65	35	43,0	200,3	4,26	2,77	3,73
680	63	37	43,7	189,7	4,26	2,77	3,71
780	62	38	44,0	176,0	4,26	2,82	3,71
890	59	41	44,0	156,3	4,26	2,83	3,68
990	58	42	45,2	128,8	4,26	2,74	3,62

*) Here are values for ^{97}Zr ,
for ^{131}I , ^{133}I , and ^{143}Ce the calculations are also done

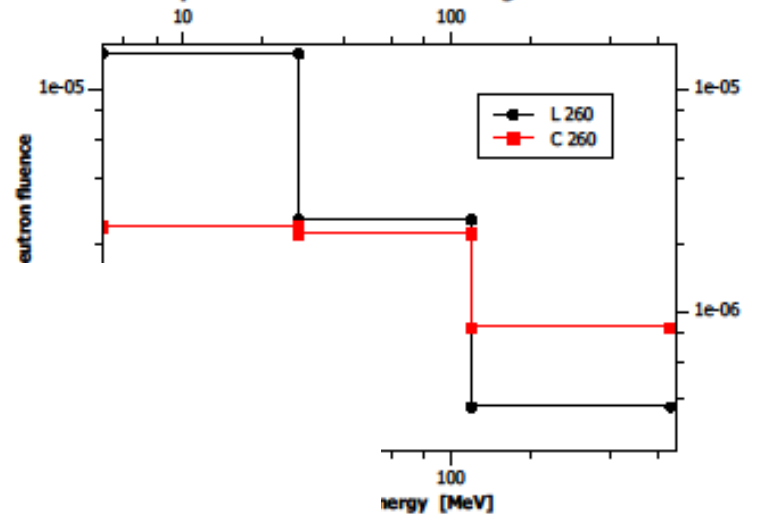




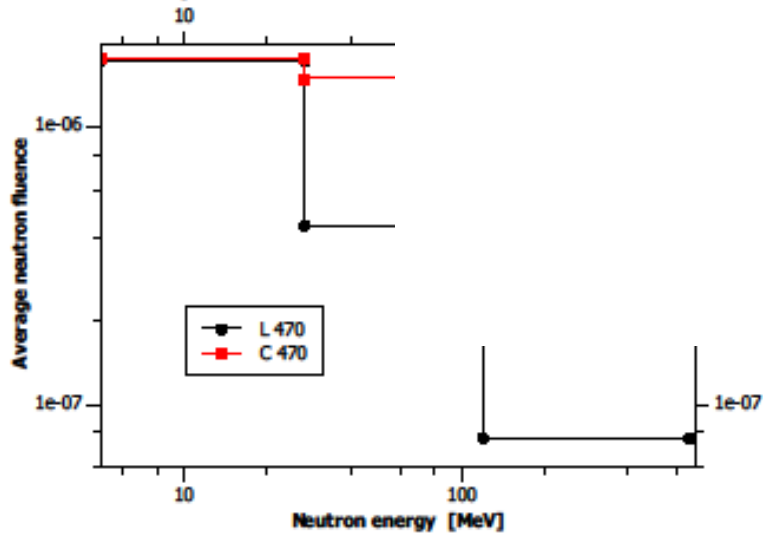
Neutron spectra Lead and Carbon Target Z=50 mm



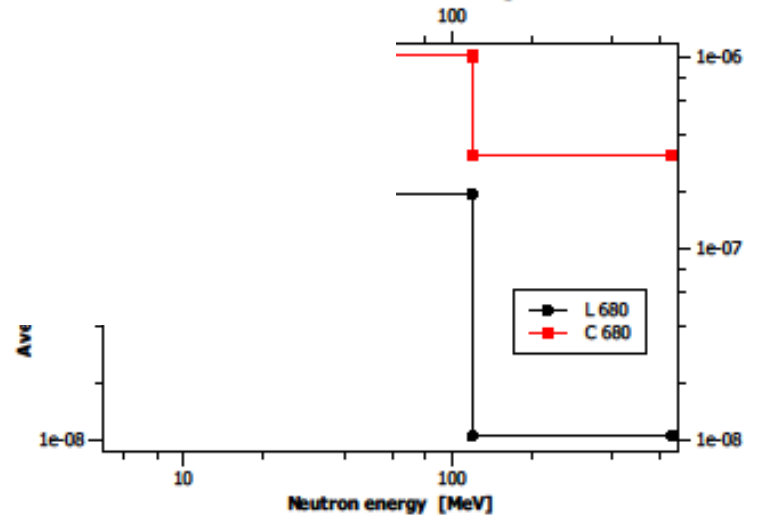
Neutron spectra Lead and Carbon Target Z = 260 mm



Neutron spektra Lead and C



Carbon Target Z = 680 mm



CONCLUSIONS

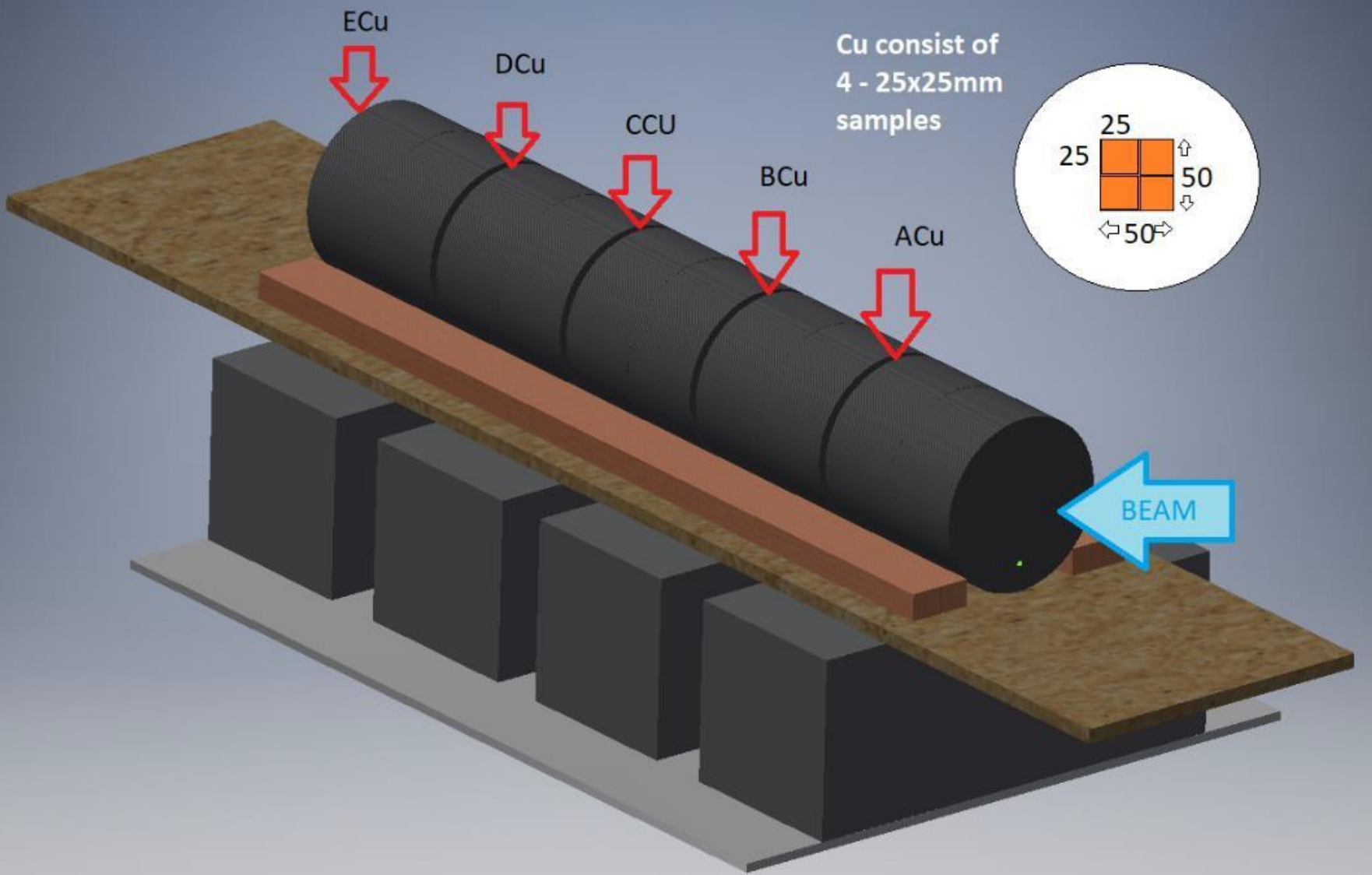
**Yields for ^{97}Zr , ^{131}I , ^{133}I , ^{143}Ce
for Carbon target we must know most precise**

**Almost 40% protons escape for Carbon
We can try propose configuration
Lead + Carbon**

**We must finished calculation of neutron
spectra for all samples of Ud and threshold
detector**

**It interesting to study experimentaly
Be target with diameter 190 mm and length 1000 mm**

THANK YOU
FOR YOUR
ATTENTION!



Target «Quinta-M»

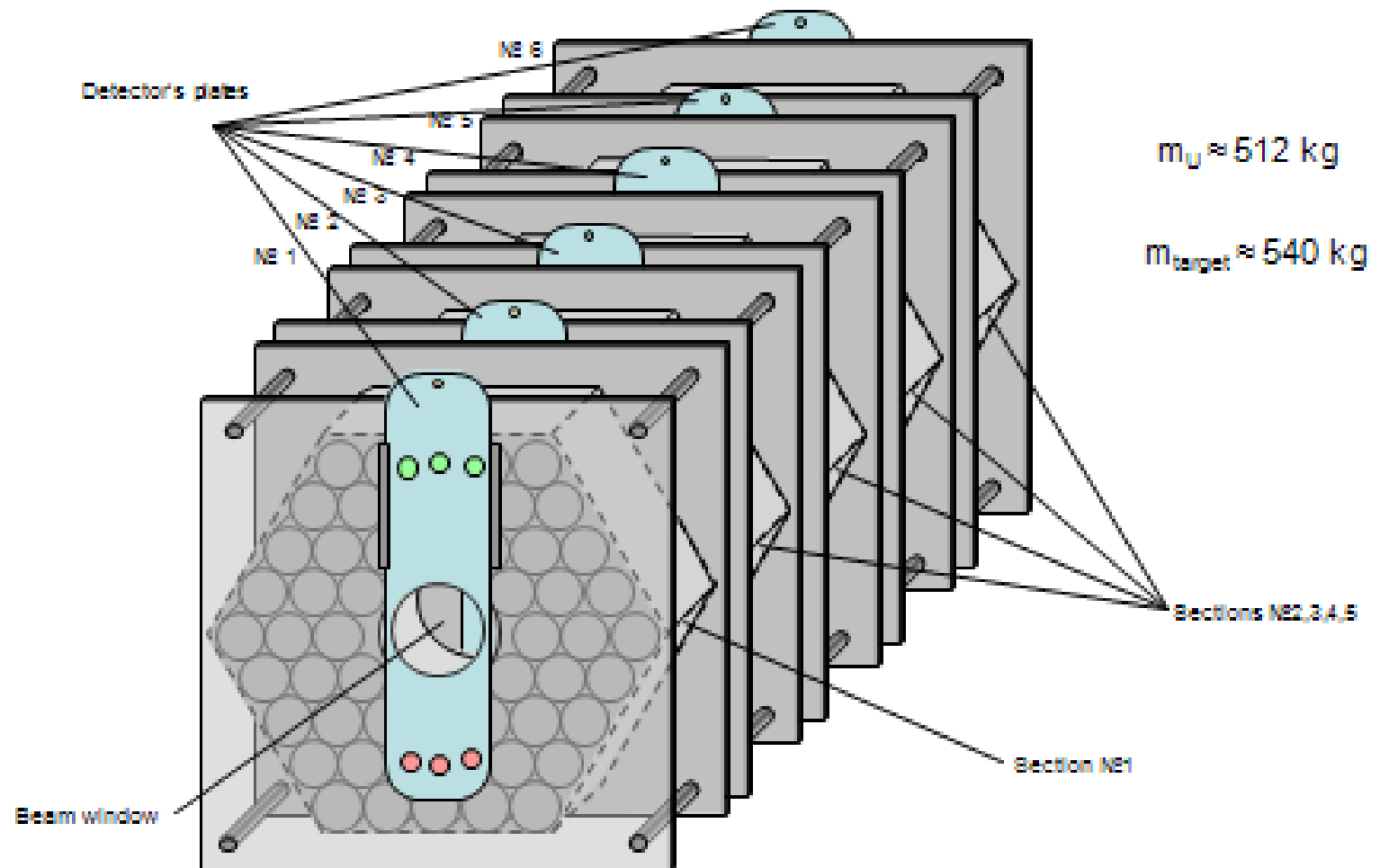
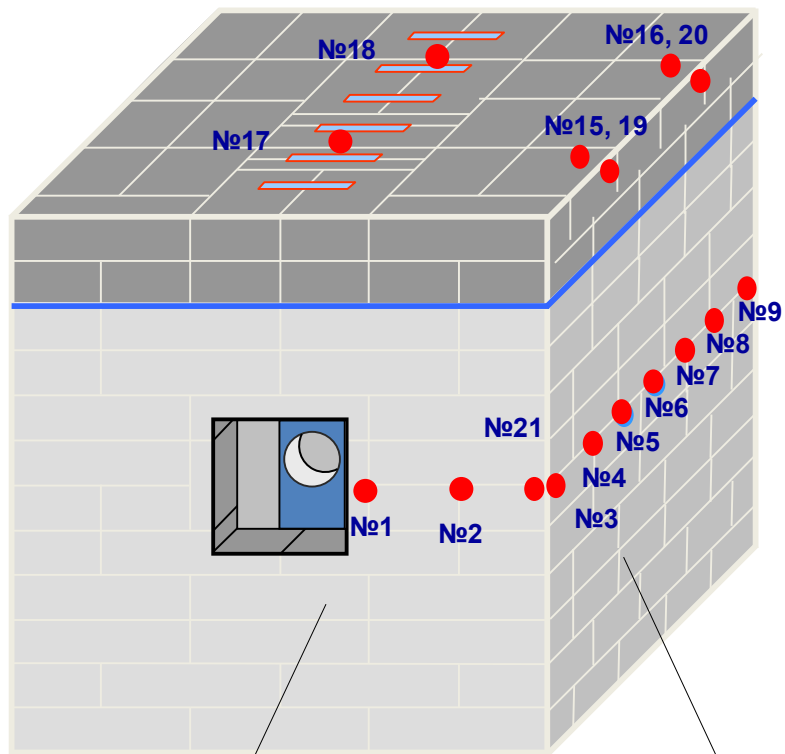


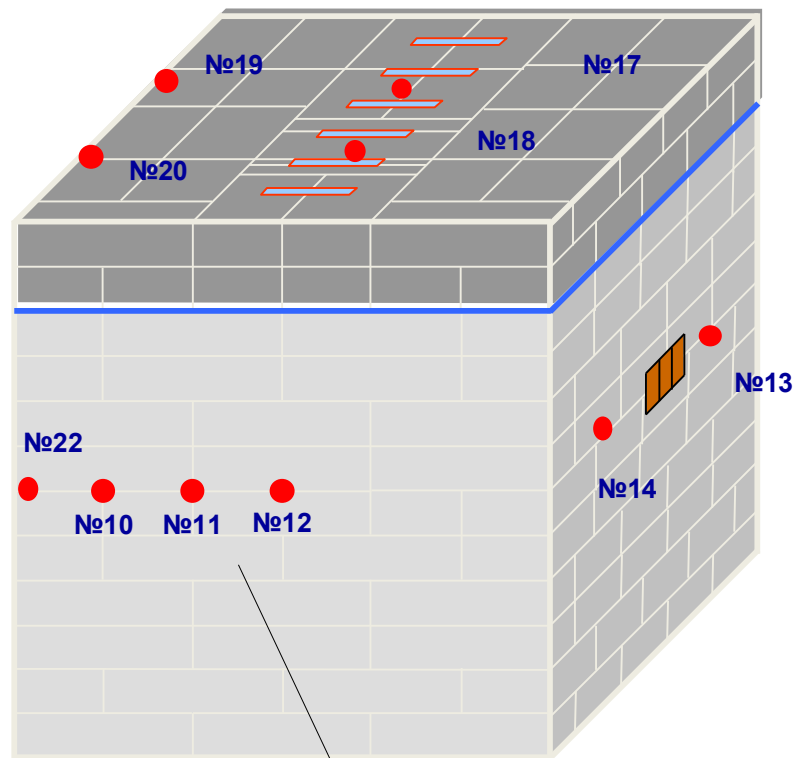
Fig. 1

Схема расположения АI-детекторов на поверхности свинцовой сборки установки «Квинта»



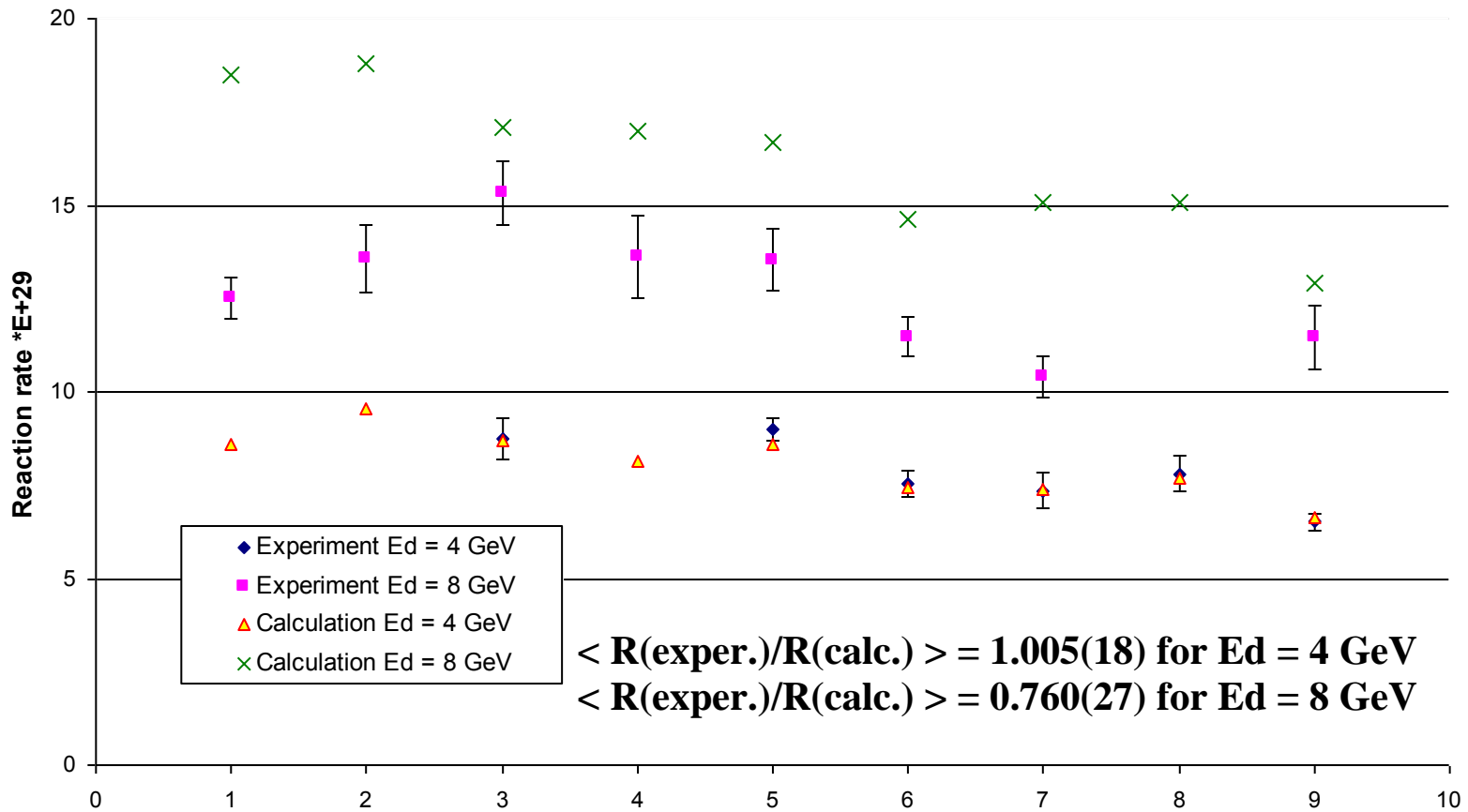
Передняя поверхность

Боковая поверхность

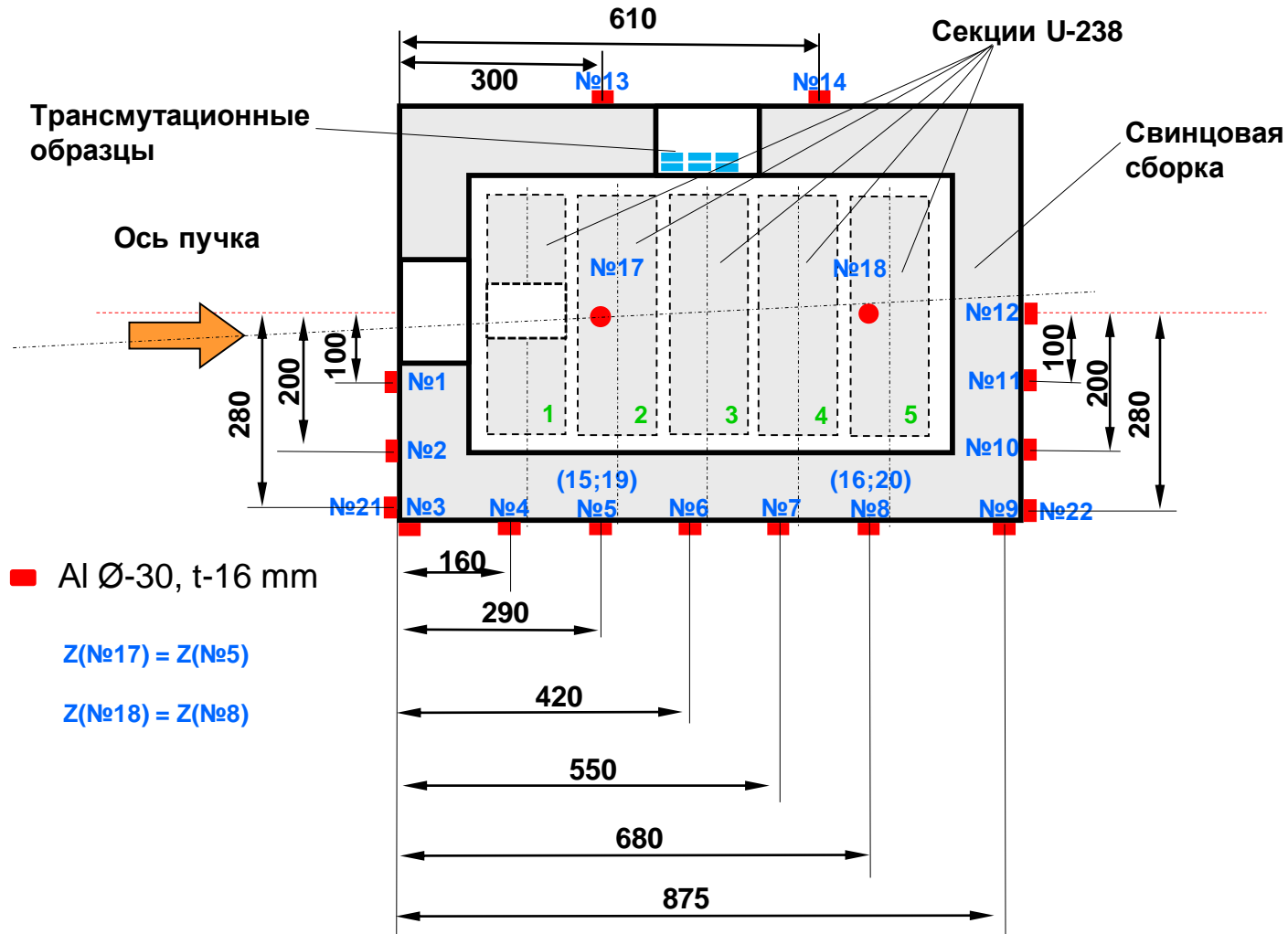


Задняя поверхность

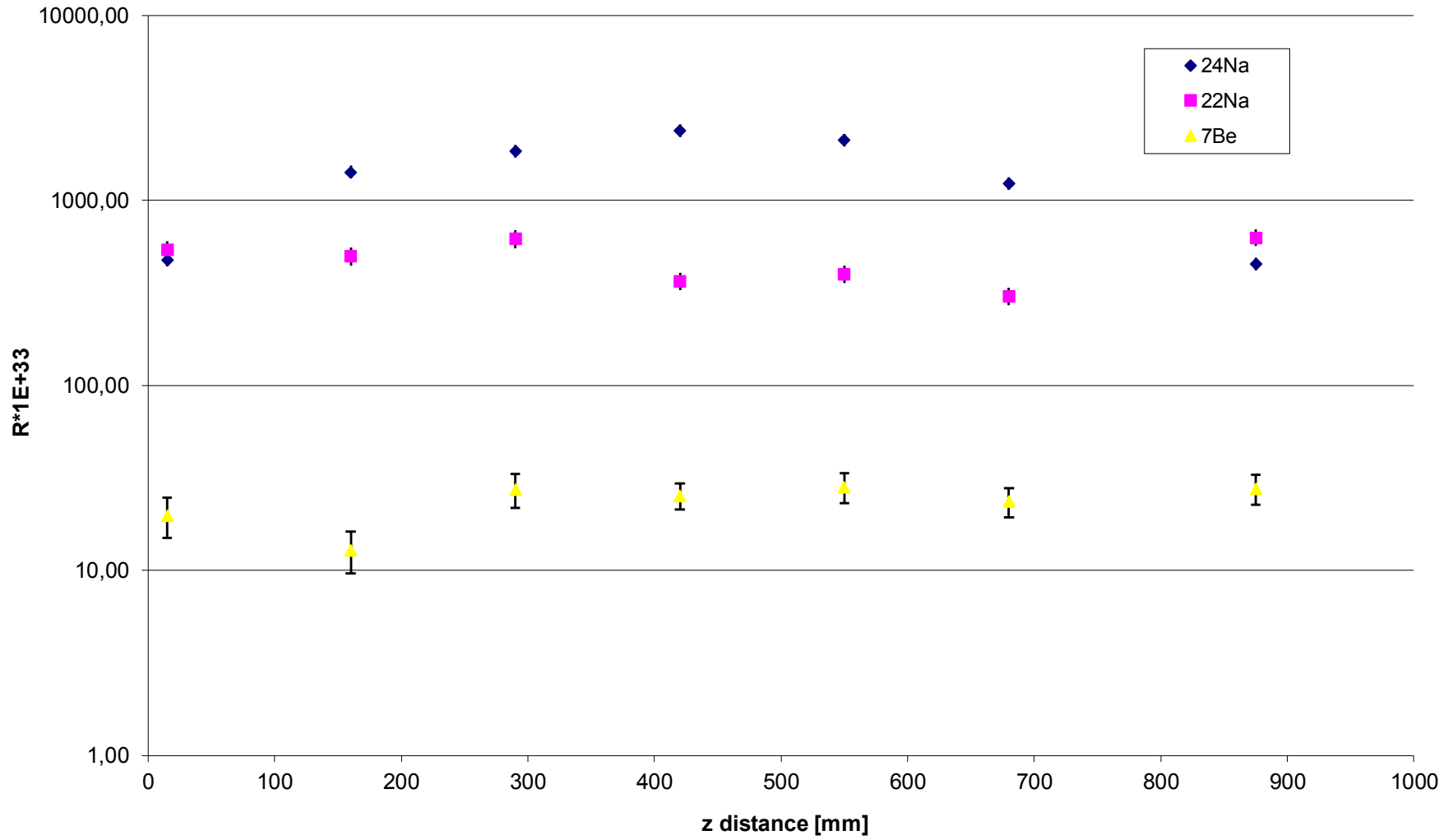
REACTION RATE $^{27}\text{Al}(n,\dots)^{24}\text{Na}$



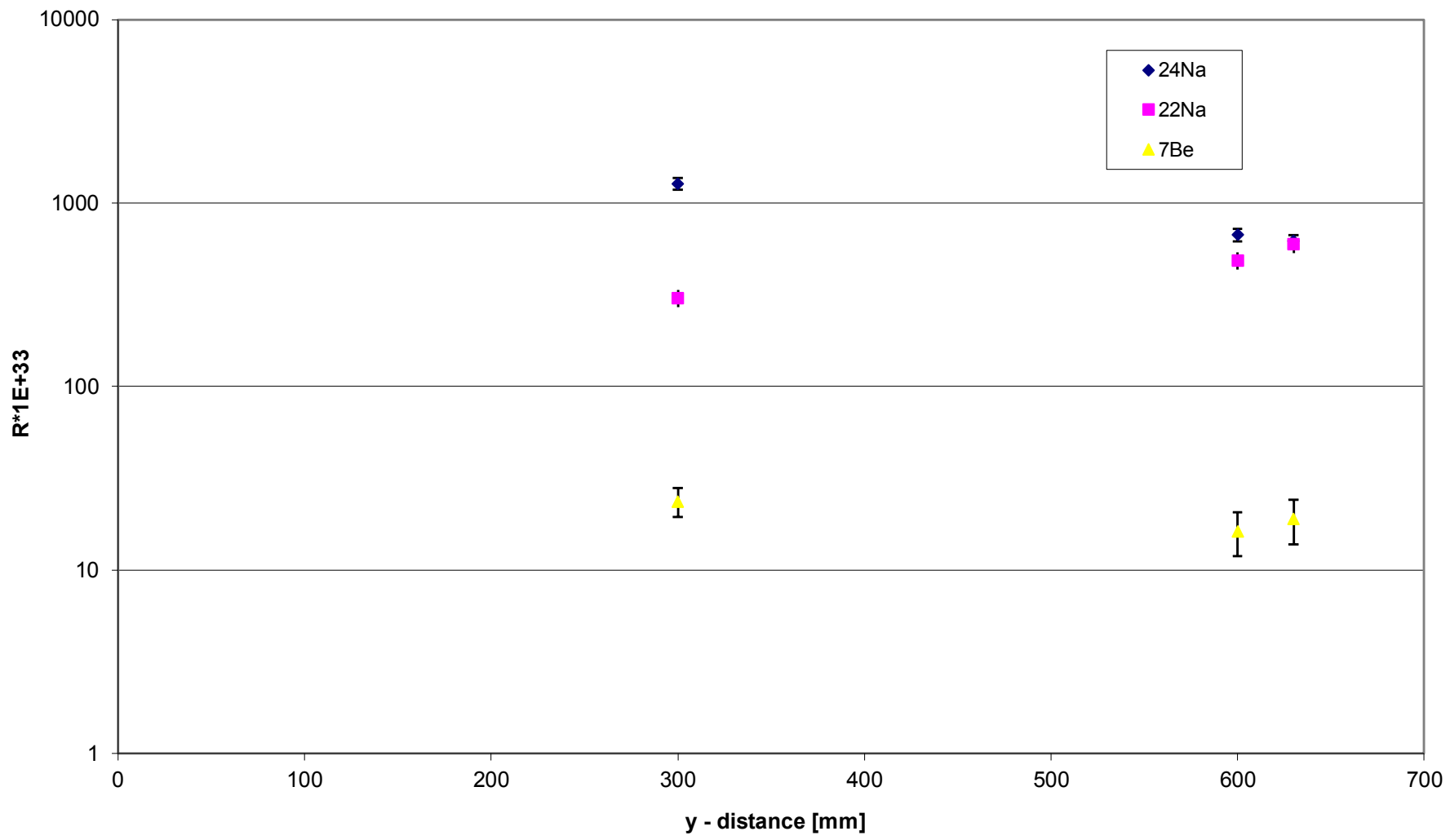
Расположение Al-детекторов на поверхности свинцовой сборки установки «Квинта» (Крышка установки условно не показана).



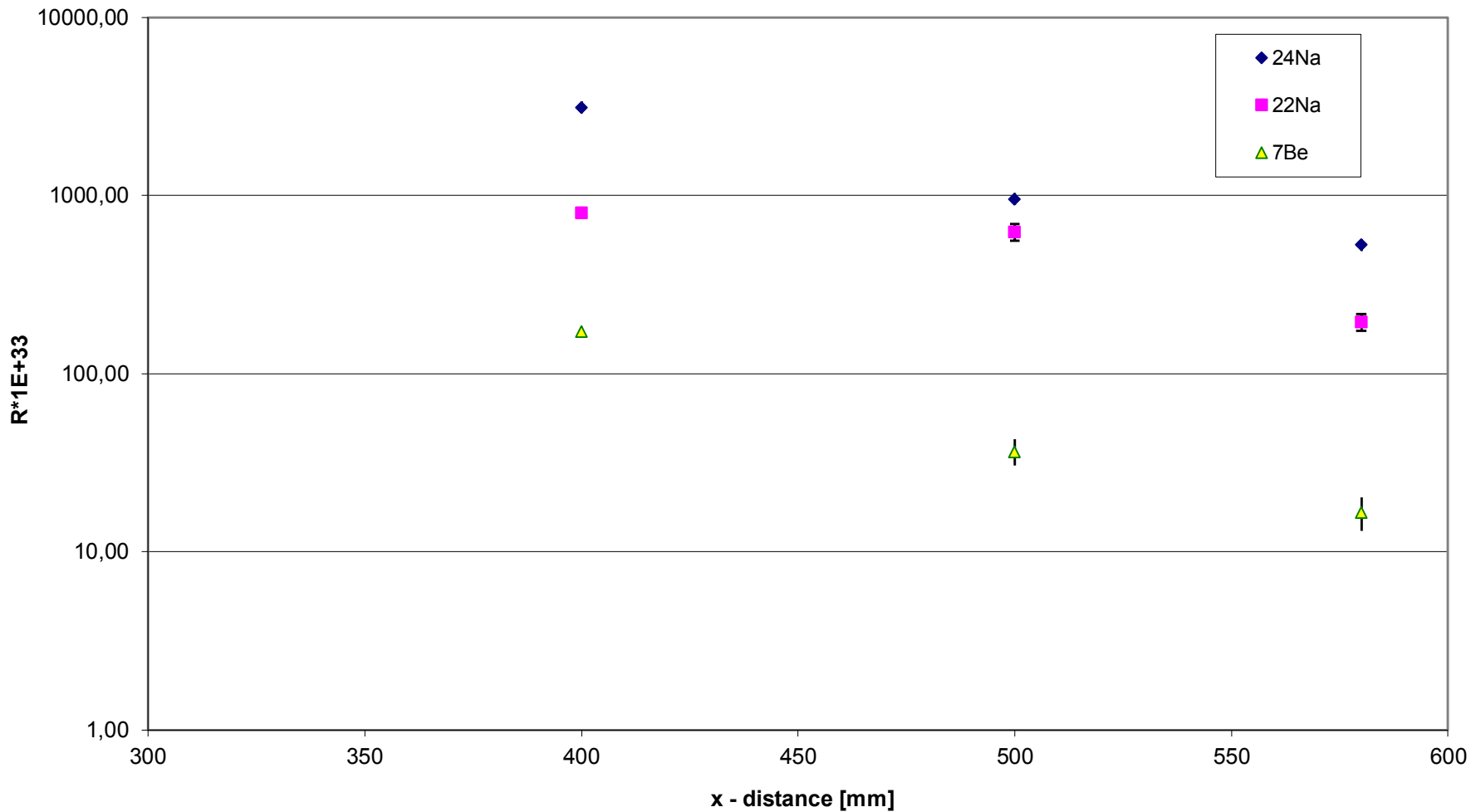
R - Rates of reaction products in $^{27}\text{Al} (n,x)^{24}\text{Na}$, ^{22}Na , ^7Be
Right side, z - dependence



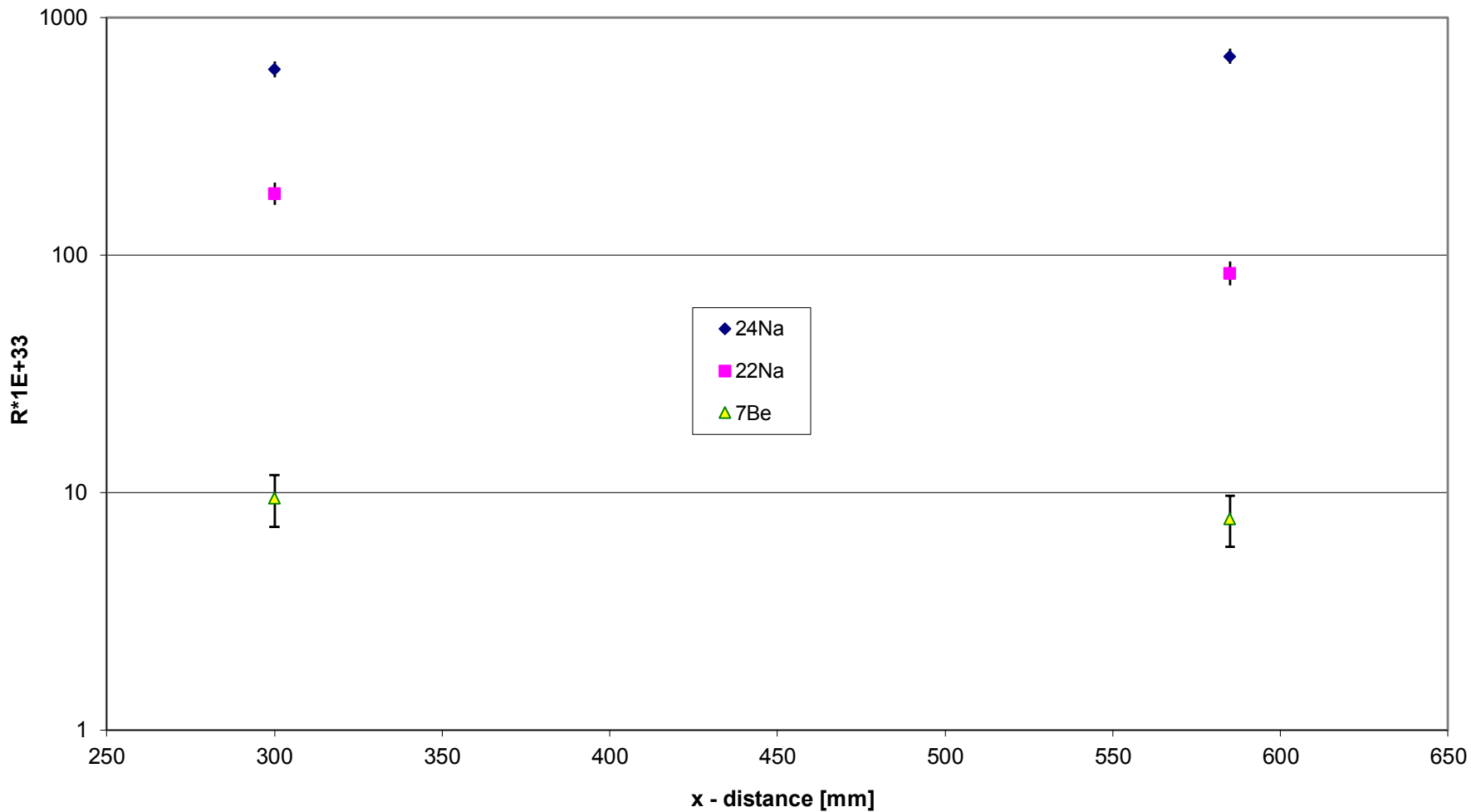
R - Rates of reaction products in $^{27}\text{Al}(n,x)^{24}\text{Na}$, ^{22}Na , ^7Be
Right side, y - dependence



**R - Rates of reaction products in $^{27}\text{Al}(n,x)^{24}\text{Na}$, ^{22}Na , ^7Be
Before side, x - dependence**



**R - Rates of reaction products in $^{27}\text{Al}(n,x)^{24}\text{Na}$, ^{22}Na , ^7Be
Top side, x - distance, y = 615 mm, z = 290 mm**



R - Rates of reaction products in $^{27}\text{Al}(n,x)^{24}\text{Na}$, ^{22}Na , ^7Be
Top side, z - distance, x = 300 mm, y = 615 mm



Reaction rate for $^{27}\text{Al}(n,\dots)^{24}\text{Na}$, $^{27}\text{Al}(n,\dots)^{22}\text{Na}$ and $^{27}\text{Al}(n,\dots)^7\text{Be}$ experimental and calculated

Resid. nuclei	Data	Ed = 4 GeV		Ed = 8 GeV		R(8GeV)/R(4GeV)
		R [E-29]	d(R) [E-29]	R [E-29]	d(R) [E-29]	
Na24	Exper.	7.48	0.43	12.23	0.54	1.64(12)
	Calcl.	7.473		16.75		2.24
	Exp/cal	1.00	0.06	0.73	0.03	
Na22	Exper.	0.522	0.029	2.73	0.22	5.23(51)
	Calcul.	0.71		1.73		2.43
	Exp/cal	0.73	0.04	1.58	0.13	
Be7	Exper.	0.069	0.011	0.471	0.083	6.84(150)
	Calcul.	0.0274		0.0736		2.69
	Exp/calc	2.51	0.38	6.40	1.13	

Calculation of average neutron fluence from reaction reaction rate of Be-7, Na-22 and Na-24

$$R_3 = \int_3^4 \sigma_3(E) \phi_3(E) dE \cong \phi_3 \sum_3^4 \sigma_3(E) \Delta E = \phi_3 X_{34}(3)$$

$$R_3 = F_3 * X_{34}(3)$$

$$R_2 = F_2 * X_{23}(2) + F_3 * X_{34}(2)$$

$$R_1 = F_1 * X_{12}(1) + F_2 * X_{23}(1) + F_3 * X_{34}(1)$$

$$F_3 = R_3 / X_{34}(3)$$

$$F_2 = (R_2 - F_3 * X_{34}(2)) / X_{23}(2)$$

$$F_1 = (R_1 - F_2 * X_{23}(1) - F_3 * X_{34}(1)) / X_{12}(1)$$

Sum of cross-section

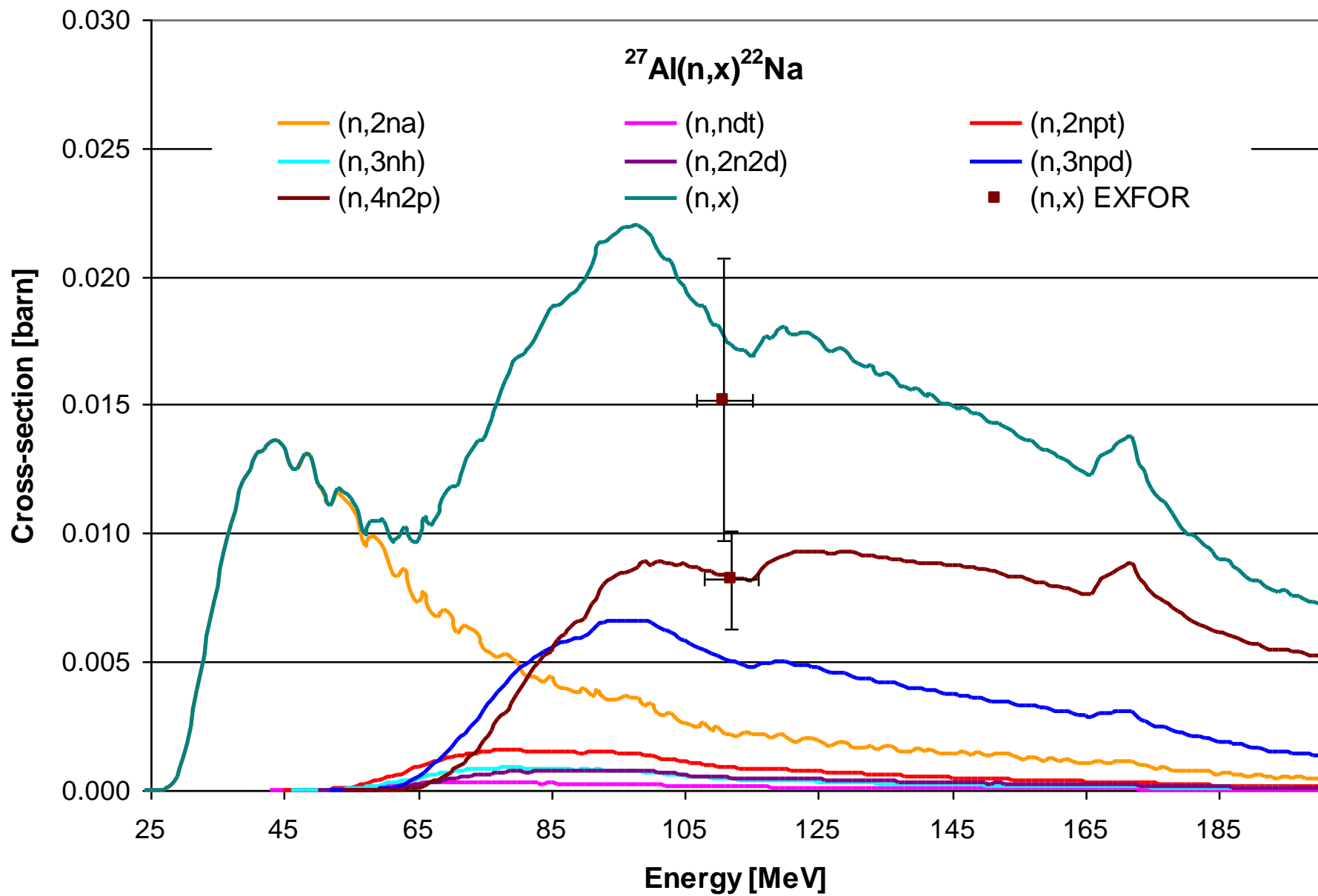
X12(1)

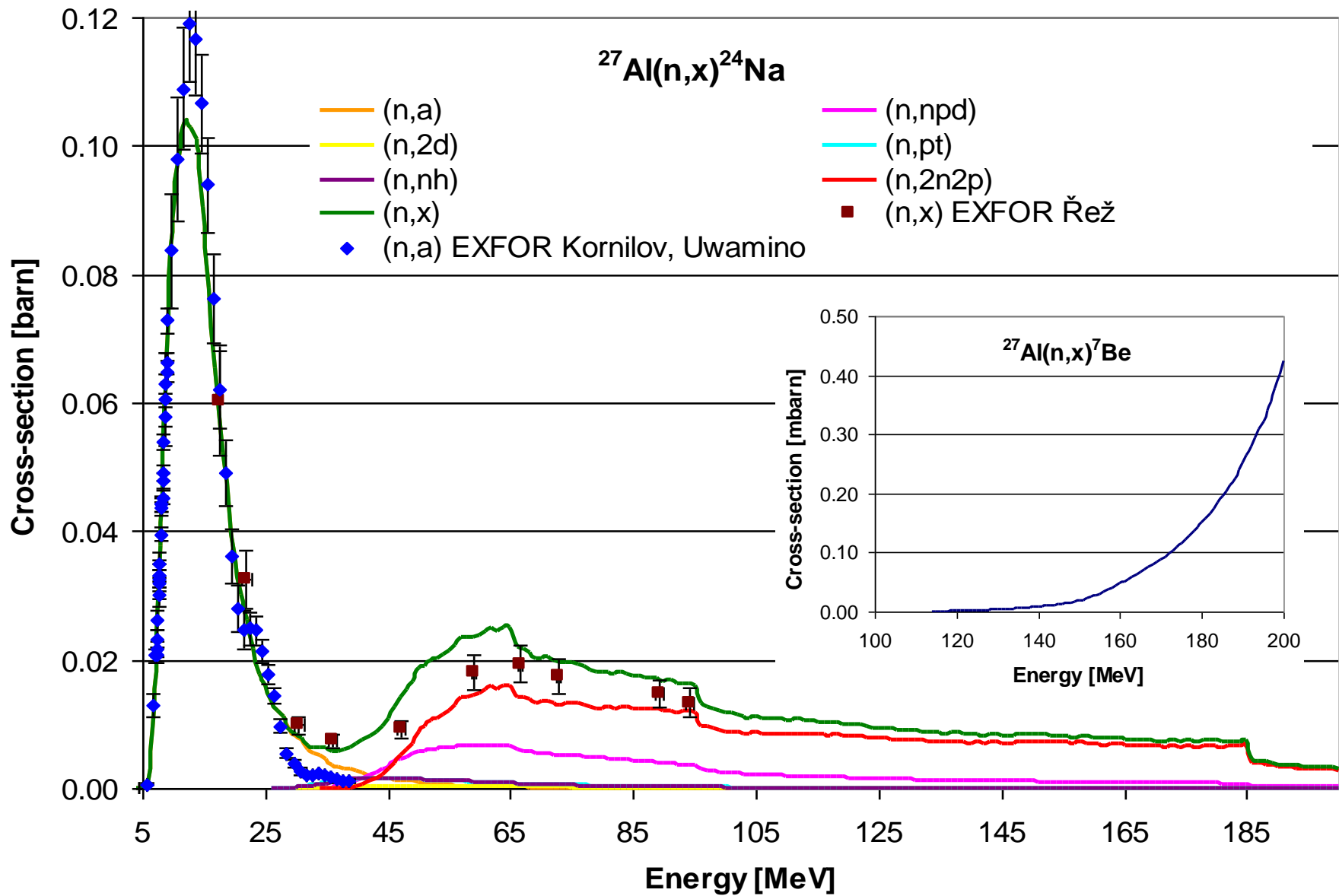
X23(i)

X34(i)b

X34(i)c

Residual Nuclei	Threshold [MeV]	No.	5->27 [barn]	27->119 [barn]	119->800 [barn]	119->1000 [barn]
24Na	5	1	1.12	1.38	1.925	3.132
22Na	27	2		1.32	7.891	10.690
7Be	119	3			5.386	7.663





**Measured average neutron fluences
[neutrons/(cm².MeV.deuteron)] x10⁻⁵**

in case of two beam energies, 4 and 8 GeV

Product	Data	E_d = 4 GeV Fluence ϕ [E-5]	E_d = 8 GeV Fluence ϕ [E-5]	ϕ (8GeV)/ϕ(4GeV)
²⁴Na	Exp.	4.734(243)	8.521(511)	1.800
	Calc.	5.160	12.91	2.502
	exp/calc	0.917	0.660	
²²Na	Exp.	0.182(12)	0.851(69)	4.676
	Calc.	0.261	0.550	2.107
	exp/calc	1.077	2.706	
⁷Be	Exp.	0.0358(57)	0.150(27)	4.190
	Calc.	0.00748	0.00749	0.999
	exp/calc	4.786	20.03	

Results of analysis of γ -ray spectra of $U_{nat.}$ after irradiation with secondary neutrons from $E_d = 1.60$ GeV. All corrections are included. (+) denotes mixing due to other nuclide.

Isotope Energy[keV]	Activity[Bq] I_g [%]	$T_{1/2}$ (Library) $T_{1/2}$ (Exper.)	 B	<R> R	Number of spectra
Np-239	849(40)	2.3565(4) d	7.51(35)-05	2.97(14)E-26	31-X,16-C
106.125	27.2	2.388(15) d	6.76(30)E-05	2.67(12)E-26	6-X
106.125	27.2	2.39(6) d	6.51(40)E-05	2.64(16)E-26	3-C
209.753	3.42	2.36(5) d	9.54(43)E-05	3.77(17)E-26	5-X
209.753	3.42	2.44(10) d	9.00(52)E-05	3.56(21)E-26	3-C
228.183	10.76	2.45(6) d	8.86(37)E-05	3.50(15)E-26	6-X
228.183	10.76	2.49(4) d	8.51(54)E-05	3.36(21)E-26	3-C
277.599	14.38	2.35(3) d	7.37(33)E-05	2.91(13)E-26	5-X
277.599	14.38	2.45(9) d	7.47(53)E-05	2.96(21)E-26	3-C
315.879	1.60	1.8(3) d	7.70(63)E-05	3.04(25)E-26	4-X
315.879	1.60	2.30(12)d	7.12(64)E-05	2.81(25)E-26	2-C
334.309	2.07	2.04(14) d	6.25(52)E-05	2.47(21)E-26	5-X
334.309	2.07	3.2 d	5.15(51)E-05	2.03(20)E-26	2-C
Mo-99	14.1(16)	2.7475(4) d	1.45(17)E-06	5.74(65)E-28	3;7X,7C
Te-132	11.5(10)	3.204(2) d	1.38(12)E-06	5.46(46)E-28	7;12X,18C
I-133	35(18)	20.8(1) h	8.0(41)E-07	3.2(16)E-28	1;2X,2C
I-135	175(14)	6.57(2) h	1.80(26)E-06	7.13(57)E-28	6;6C
Xe-135	152(58)	9.14(2) h	2.04(109)E-06	8.6(38)E-28	1;3X,2C
Ba-140	3.38(10)	12.752(3) d	1.62(5)E-06	6.40(19)E-28	5;1X,15C
Ce-143	24.5(54)	33.039(6) h	1.26(27)E-06	5.0(11)E-28	3;4X,7C

Group weight factors for calculations of total number of fissions

$$w_j(t) = \frac{\int_{a(j)}^{a(j+1)} \sigma_j(t, E_n) \Phi(E_n) dE_n}{\int_{a(1)}^{a(4)} \sigma_j(t, E_n) \Phi(E_n) dE_n} \quad (16)$$

- * thermal, epithermal and resonance – from $a(1) = 10^{-5}$ eV to $a(2) = 126$ keV
- * unresolved resonance and fast – from $a(2) = 126$ keV to $a(3) = 4.57$ MeV
- * fast and high energy neutrons – from $a(3) = 4.57$ MeV up to $a(4) =$ beam energy

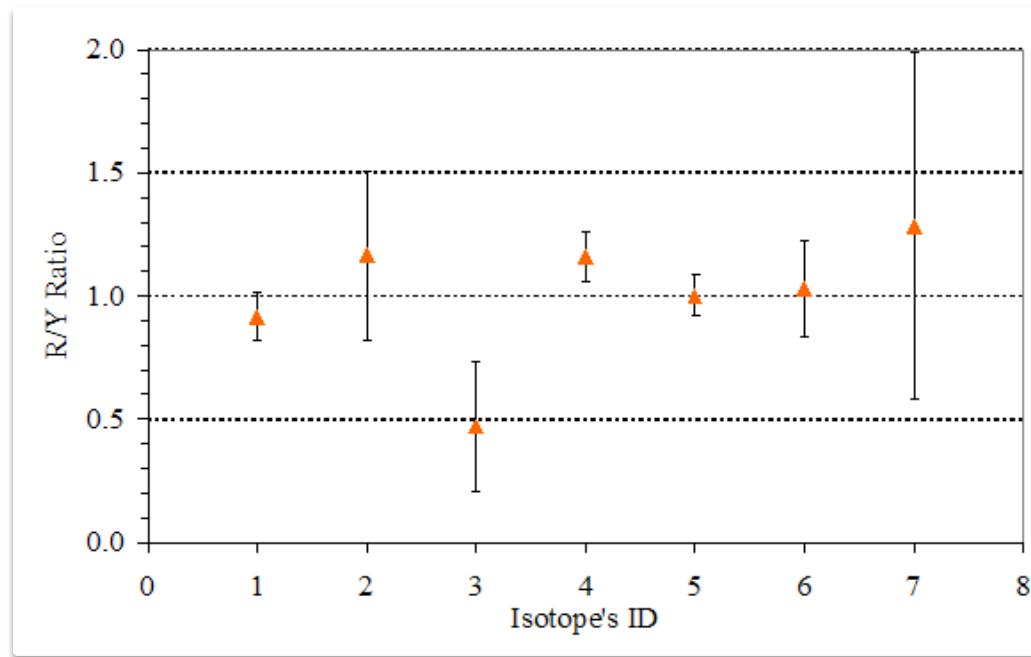
$$Y_{\text{cum}}(\text{Th}, {}^{99}\text{Mo}) = w_2(\text{Th}) \cdot Y_{\text{cum}}(\text{Th}, {}^{99}\text{Mo}, 2) + w_3(\text{Th}) \cdot Y_{\text{cum}}(\text{Th}, {}^{99}\text{Mo}, 3)$$

$$Y_{\text{cum}}(\text{U}_{\text{nat}}, r) = [0.007204 (w_1({}^{235}\text{U}) \cdot Y_{\text{cum}}({}^{235}\text{U}, r, 1) + w_2({}^{235}\text{U}) \cdot Y_{\text{cum}}({}^{235}\text{U}, r, 2) + w_3({}^{235}\text{U}) \cdot Y_{\text{cum}}({}^{235}\text{U}, r, 3))] + [0.992742 ((w_2({}^{238}\text{U}) \cdot Y_{\text{cum}}({}^{238}\text{U}, r, 2) + (w_3({}^{238}\text{U}) \cdot Y_{\text{cum}}({}^{238}\text{U}, r, 3)))]$$

where $r = {}^{99}\text{Mo}, {}^{132}\text{Te}, {}^{133}\text{I}, {}^{135}\text{I}, {}^{135}\text{Xe}, {}^{140}\text{Ba}$ and ${}^{143}\text{Ce}$.

E_n	^{232}Th	^{235}U	^{238}U	natU
Epithermal	$6.72 \cdot 10^{-7}$	0.636	$7.12 \cdot 10^{-5}$	$4.65 \cdot 10^{-3}$
Resonance	0.663	0.318	0.715	0.712
Fast	0.337	0.046	0.285	0.283

The relative ratio of $R_{\text{exp}}(^{\text{nat}}\text{U}, r) / (Y_{\text{cum}}(^{\text{nat}}\text{U}, r))$

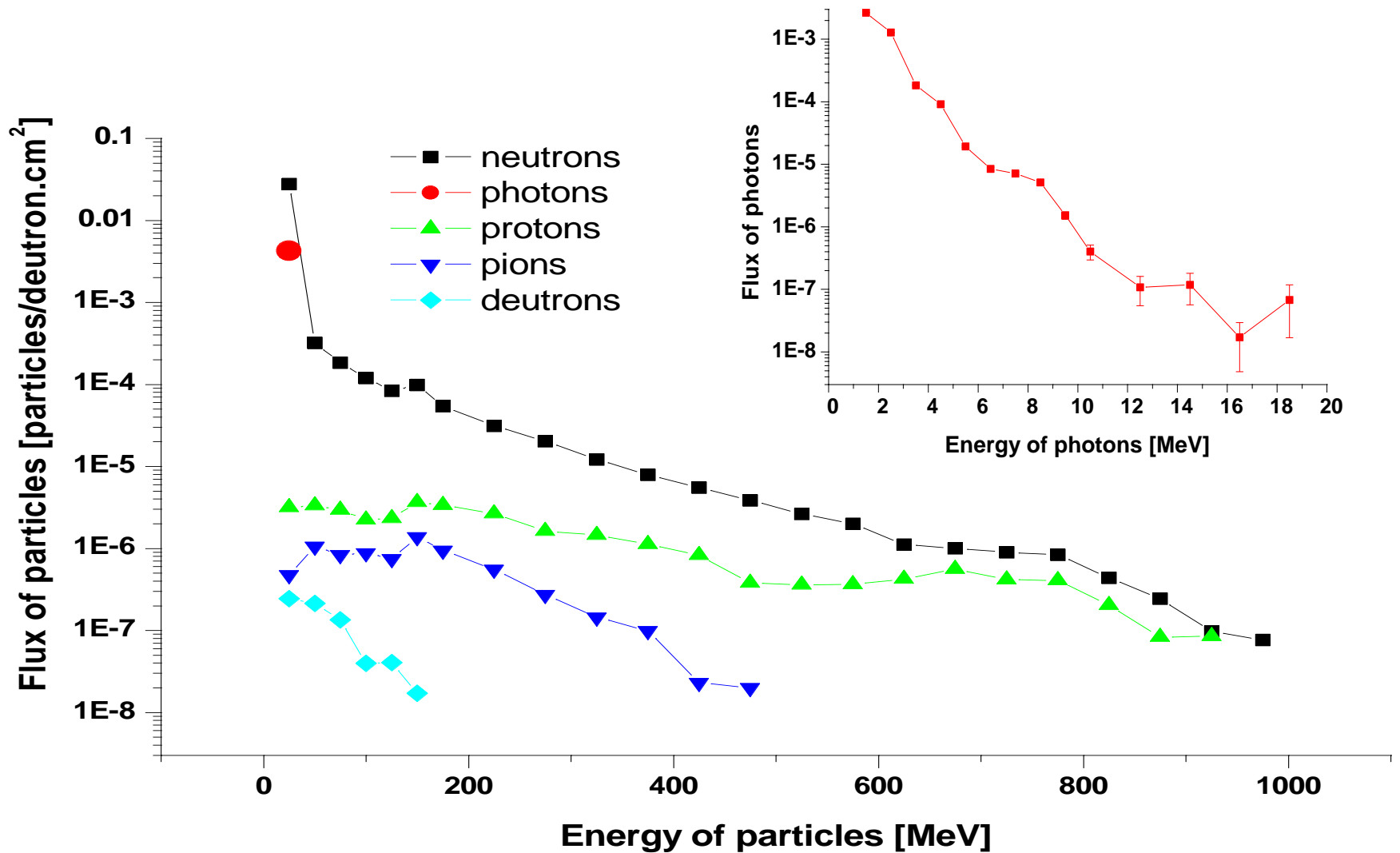


X-axis 1 = ^{99}Mo , 2 = ^{132}Te , 3 = ^{133}I , 4 = ^{135}I , 5 = ^{135}Xe , 6 = ^{140}Ba , and 7 = ^{143}Ce

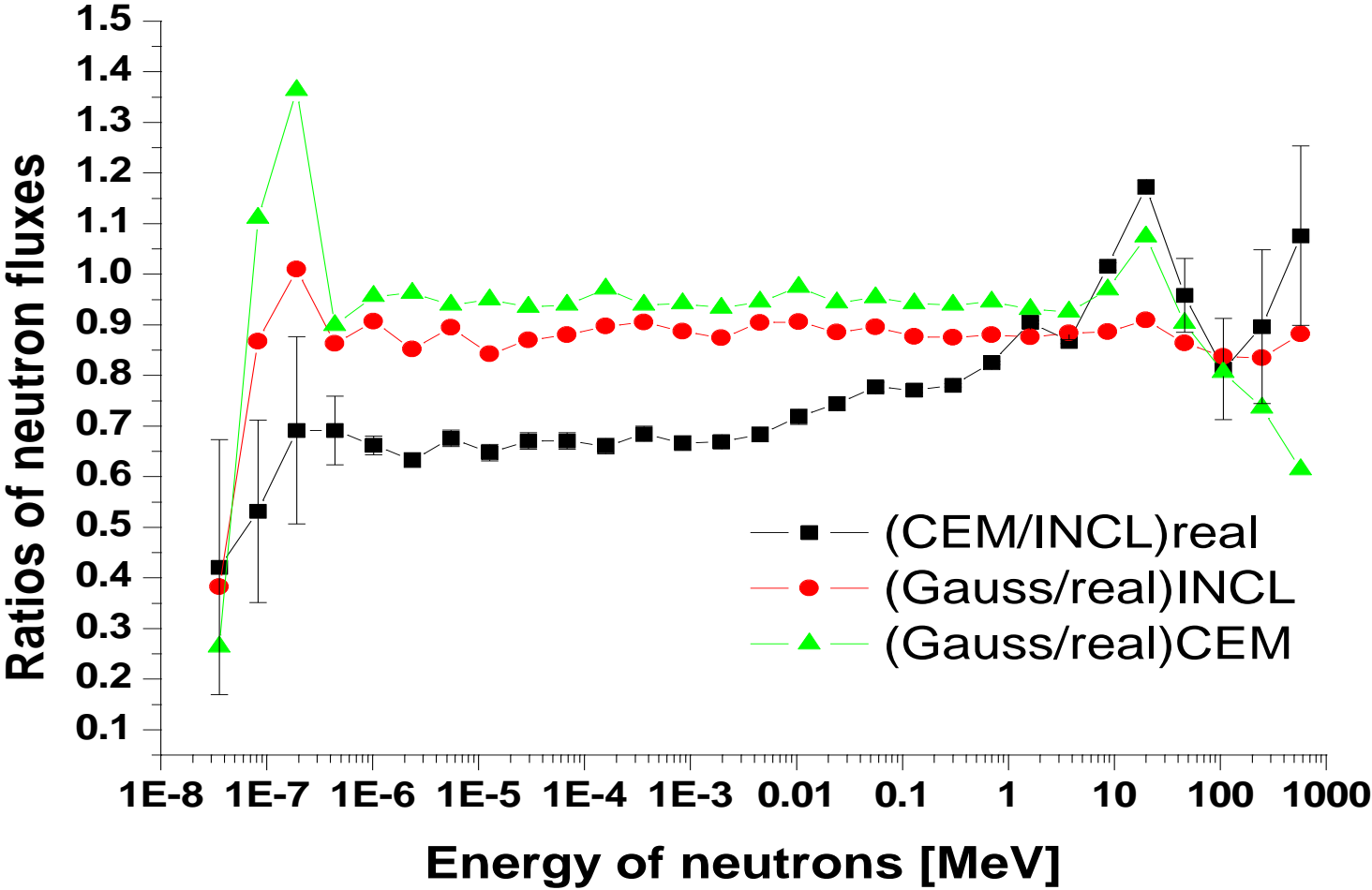
Calculation of neutron spectra and reaction rates.

- MCNPX 2.6.C
- Neutron flux, 4 cells 36*36*15 mm on top of 2nd section
- Setup: lead target, uranium rods in hexagonal lattice, polyethylene box with cadmium shielding, metal and aluminum holders and wooden plates
- Realistic size of beam: $X_c = -0.64$ cm, $Y_c = -0.39$ cm, FWHM – $X = 2.87$ cm, $Y = 1.92$ cm
Gauss: $X_c = Y_c = 0$, FWHM – $X = Y = 4.00$ cm
- CEM, INCL model with the LA150N and LA150H libraries
- $3.2 \cdot 10^7$ of incident particles were used for each calculation

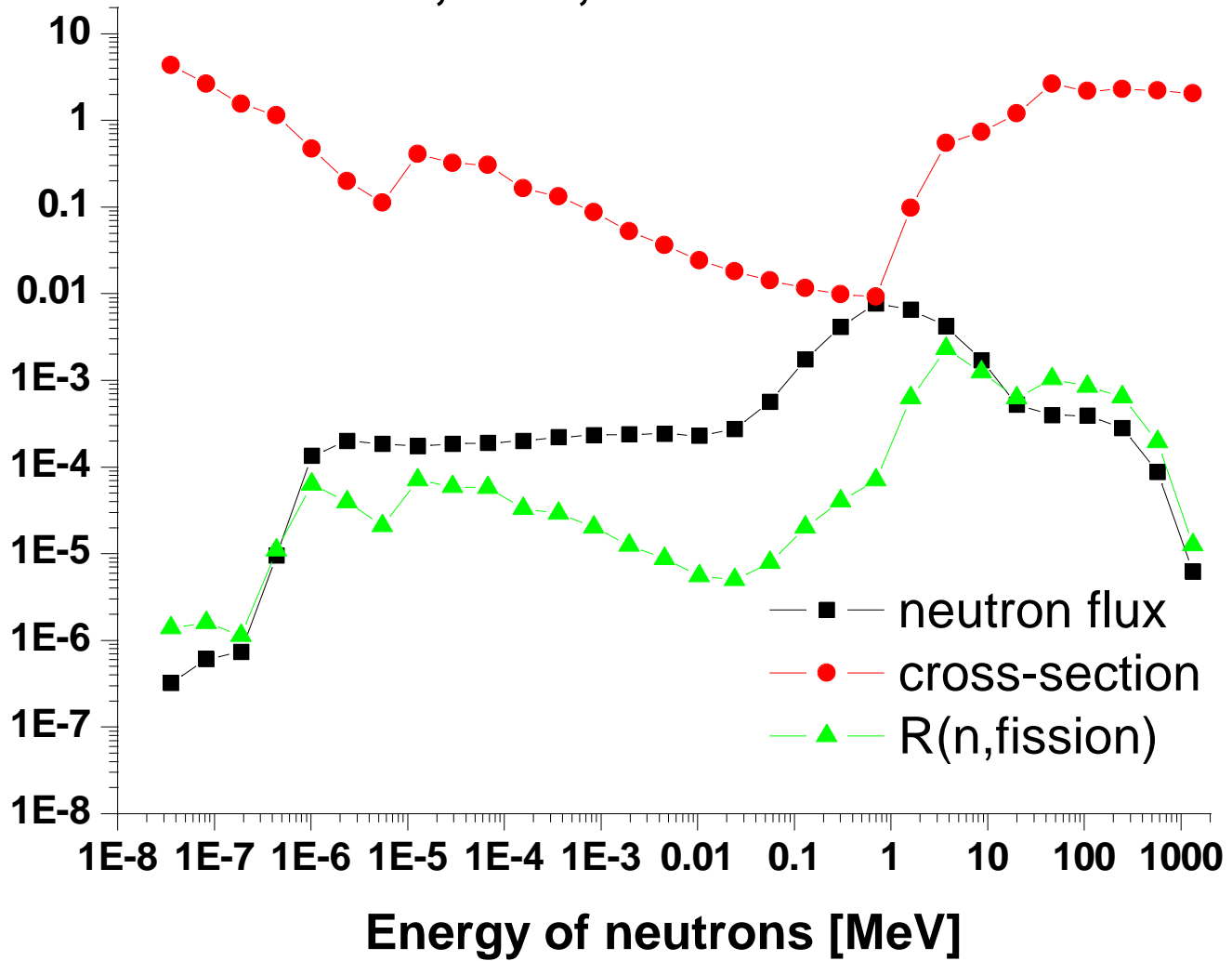
The simulated particles spectra on top of second section of our setup using “INCL” model and “real” beam

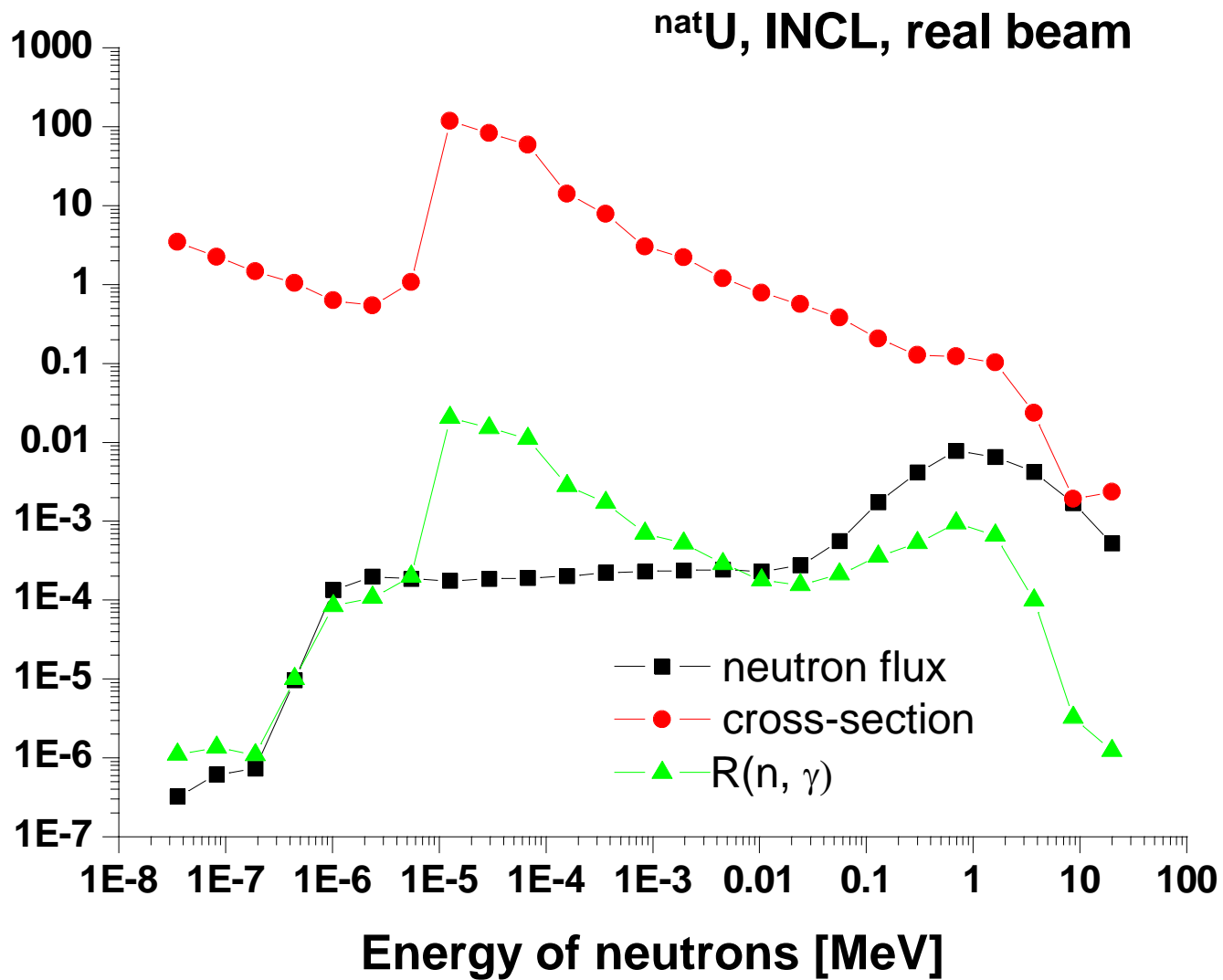


Ratio of neutron flux simulated in box 3 (uran) with different combination of intra-nuclear model and shape of beam.



^{nat}U, INCL, real beam





	232Th			Unat	
Reaction	(n,g)	(n,f)	(n,2n)	(n,g)	(n,f)
Reaction Rate, exper.	3.03(10)E-26	5.89(60)E-27	1.60(16)E-27	2.97(14)E-26	2.24(10)E-26
R(CEM-Gauss)	2.35E-26	2.38E-27	9.95E-28	5.87E-26	1.02E-26
R(CEM-real)	1.75E-26	1.83E-27	1.16E-27	3.66E-26	7.26E-27
R(INCL-Gauss)	2.74E-26	2.10E-27	1.09E-27	5.16E-26	7.80E-27
R(INCL-real)	2.49E-26	2.03E-27	1.06E-27	5.49E-26	7.93E-27
R(C-G)/R(C-r)	1.34	1.30	0.86	0.62	1.40
R(C-G)/R(I-r)	0.94	1.17	0.94	1.07	1.29
R(C-r)/R(I-r)	0.70	0.77	1.09	0.67	0.92
R(I-G)/R(I-r)	1.10	1.04	1.03	0.94	0.98
R(exper.)/R(I-r,calc.)	1.22(4)	2.90(30)	1.51(15)	0.54(3)	2.82(13)

C-G sign CEM-Gauss, C-r _ CEM-real, I-G _ INCL-Gauss, I-r _ INCL-real

$P(A_r, Z_r)$ - Transmutation rate.

$$P(A_r, Z_r) = m(A_r, Z_r) / m(A_t, Z_t)$$

$$P(A_r, Z_r) = R(A_r, Z_r) N_d(\text{integral}) (A_r / A_t)$$

With normalization to 10^9 beam particles

$$P_{\text{norm}}(A_r, Z_r) = 10^9 P(A_r, Z_r) / N_d(\text{integral})$$

^{232}Th (n, γ) ^{233}Th (β - decay, $T_{1/2} = 22.3$ min) \rightarrow ^{233}Pa (β - decay, $T_{1/2} = 26.967$ d) \rightarrow ^{233}U

^{232}Th (n,2n) ^{231}Th (β -, 25.52 h) \rightarrow ^{231}Pa (β -, 32760 y) \rightarrow ^{231}U (n, γ) \rightarrow ^{232}U ($T_{1/2} = 68.9$ y)

^{238}U (n, γ) ^{239}U (β -, 23.4 min) \rightarrow ^{239}Np (β -, 2.4 d) \rightarrow ^{239}Pu (alpha, 24110 y) \rightarrow ^{235}U

Reaction	our		TARC	
	$P_{\text{norm.}}$ [10^{-17} g/g]	D_c [cm]	$P_{\text{norm.}}$ [10^{-17} g/g]	D_c [cm]
$^{232}\text{Th}(n,\gamma)$	3.09(13)	13.1	3.8(3)	122
			1.0(2)	150
$^{238}\text{U}(n,\gamma)$	2.87(9)	13.8	1.1(3)	107
			7.7(2)	94

Reaction $^{232}\text{Th}(n,2n)^{231}\text{Th}$

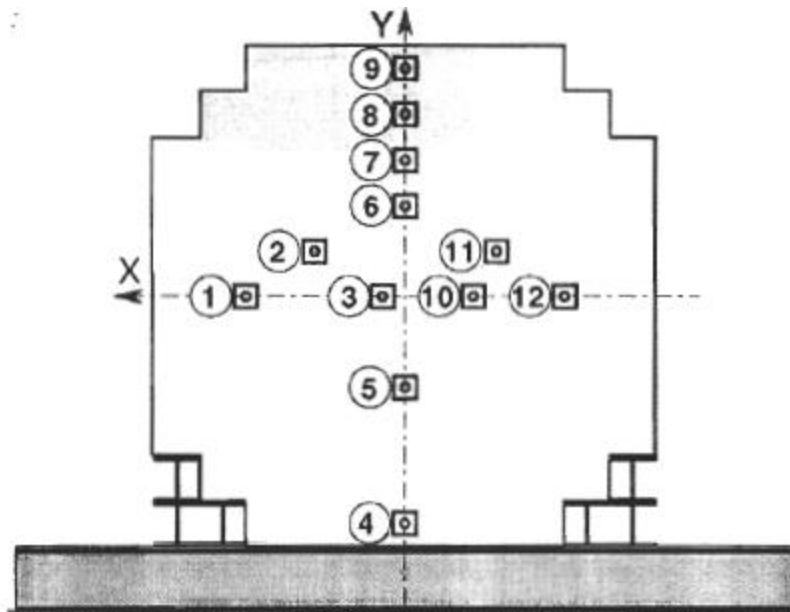
E_γ [keV]	our		TARC	
	B [10^{-6}]	D_c [cm]	B [10^{-6}]	D_c [cm]
25.646	3.96(51)	13.1	0.635(63)	4.0
84.216	4.47(65)		1.32(13)	
25.646			1.05(16)	8.5
84.216			2.11(32)	

$$P_{\text{norm}}(^{231}\text{Th}) = 1.59(15)10^{-18} \text{ [g/g] our}$$

	Th - foils			Unat. - foils	
	our	TARC		our	TARC
	(n, γ), (n, 2n)	(n, γ)	(n, 2n)	(n, γ)	(n, γ)
Weight (N o.1)(mg)	93.2	132	158	172	290
Weight (N o.2)(mg)			678		
Diameter (N o.1)(mm)	15	12.7	12.5	15	12.7
Square (N o.2)(mm)			30x29		
Thickness (N o.1)(μm)	45.0	88.9	110.3	52.0	127
Thickness (N o.2)(μm)			66.5		
Activity (N o.1)(Bq)	378	536	624	2244	3783
Activity (N o.2)(Bq)			2753		
Radial distance (N o.1) Center - sample [mm]	131	1220	~ 40	138	1070
Radial distance (N o.2) Center – simple(mm)		1500	~ 85		940
Beam particle	deuteron	proton	proton	deuteron	proton
Beam energy	1.6 GeV	3.5 GeV /c	2.5 GeV /c	1.6 GeV	3.5 GeV /c
Sum of particle	1.93.10¹³	2.14.10¹³		1.93.10¹³	2.14.10¹³
Sum of particle (No.1)			4.80.10¹²		
Sum of particle (No.2)			9.01.10¹²		
Irradiation time (h)	6.65	8.5		6.65	8.5

TARC – Transmutation by Adiabatic Resonance Capture

The 334 t lead assembly, ~ cylinder diam. 3.3 m and length 3m



Summary of the coordinates of the centres of the 12 instrumented holes in the 334 t lead assembly volume. The beam is introduced through a 77.2 mm diameter and 1.2 m long blind hole

Hole no.	x (m)	y (m)	Hole no.	x (m)	y (m)
1	1.05	0.00	2	0.60	0.30
3	0.15	0.00	4	0.00	-1.50
5	0.00	-0.60	6	0.00	0.60
7	0.00	0.90	8	0.00	1.20
9	0.00	1.50	10	-0.45	0.00
11	-0.60	0.30	12	-1.05	0.00

Summary:

Measurements and analyzing

32 Spectra – monitor Al, sample ^{232}Th , $^{\text{nat}}\text{U}$

133 peaks – calculated E_γ , I_γ , $T_{1/2}$ – determined
reaction products A_r , Z_r

Experimental Reaction rate

Th: ^{233}Pa , ^{231}Th , ^{99}Mo

U: ^{239}Np , ^{99}Mo , ^{132}Te , ^{133}I , ^{135}I , ^{135}Xe , ^{140}Ba , ^{143}Ce

Estimate: $R(\text{Th}(n,\text{fission}))$ and $R(\text{U}(n,\text{fission}))$

Calculation with MCNPX 2.6C – CEM, INCL, real,
Gauss. Neutron flux, Reaction rate, Th, U, (n,γ) ,
 $(n,2n)$ $(n,\text{fission})$

Calculation of Transmutation rate: Th, U with
 (n,γ) , $(n,2n)$ and comparisson with TARC data

THANK YOU
FOR YOUR
ATTENTION!